



961 St. David Street North

Functional Servicing and Stormwater Management Report

Project Location:

961 St. David Street North, Fergus, ON

Prepared for:

2687734 Ontario Inc.
766 Hespeler Road
Cambridge, ON N3H 5L8

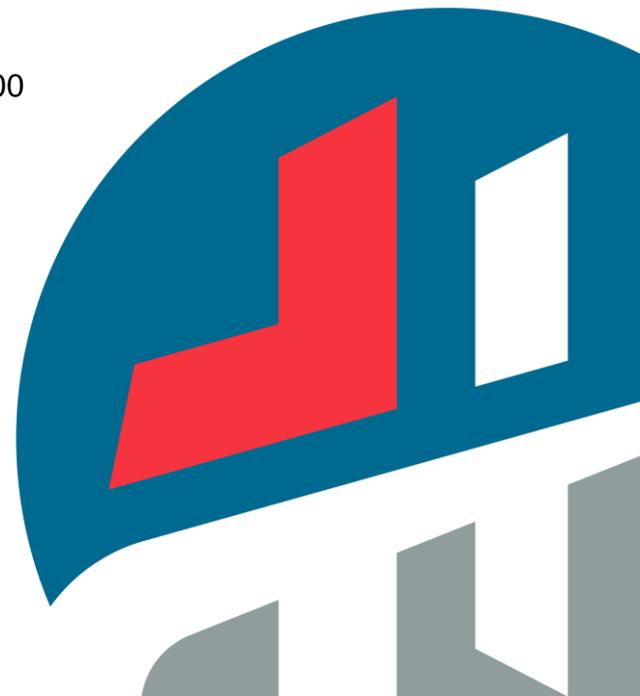
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Existing Conditions Plan MTE Drawing No. C1.1	Appended Separately
Functional Site Grading Plan MTE Drawing No. C2.1	Appended Separately
Functional Site Servicing Plan MTE Drawing No. C2.2	Appended Separately

1.0 INTRODUCTION

MTE Consultants Inc. was retained by 2687734 Ontario Inc. to complete a Functional Servicing and Stormwater Management (FSSWM) Report in support of the Zoning By-Law Amendment and Vacant Lot Condominium applications for the proposed residential development to be constructed at 961 St. David Street North/Highway 6 (herein referred to as 'the Site') in the Township of Centre Wellington.

The purpose of this study is to support the Zoning By-Law Amendment and Vacant Land Condominium applications. This will be accomplished by reviewing the opportunities and constraints for the subject property with respect to servicing, grading, and stormwater management; reviewing the requirements of the reviewing agencies; describing the development concept; and demonstrating the functional serviceability of the property. Pending approval of the applications, detailed design of the Site will commence and be submitted to the Township of Centre Wellington and other governing agencies in support of the applications and Site Plan Approval.

1.1 Site Description

The Site encompasses an area of 1.402ha, and is currently comprised of a single detached dwelling, several accessory buildings, and an asphalt driveway off 961 St. David Street North/Highway 6. The property is bounded to the west, south, and east by existing residential development, and to the northeast by St. David Street North/Highway 6. For the exact location of the Site refer to Figure 1.0.

The current zoning of the Site is Residential R1a Zone. A Zoning By-Law Amendment will be required to re-zone the Site to Residential R3 Zone to permit the proposed Vacant Land Condominium development.

1.2 Proposed Development

The proposed development for the Site is a Vacant Land Condominium, consisting of 12 single-detached houses, and 37 townhouse units, complete with a common element roadway and driveway entrance off St. David Street North/Highway 6.



961 ST. DAVID STREET NORTH



Engineers, Scientists, Surveyors

PROJECT

961 ST.DAVID STREET NORTH

TITLE

LOCATION PLAN

Drawn	JMH	Scale	1:1,500	Figure 1.0
Checked	NGK	Project No.	48650-100	
Date	2023-09-18	Rev No.	0	

2.0 EXISTING CONDITIONS

2.1 Topography

Existing topographic information for the Site was obtained from a detailed survey completed by MTE in February 2021. The Site's frontage along St. David Street North/Highway 6 has an approximate slope of 2% from west to east. There is an existing ditch along the south side of the highway along the Site's frontage, with an approximate slope of 1% from west to east. The road elevation is approximately 0.8m to 1.0m above the property line elevation along the Site's frontage. The northeast end of the Site is sloped towards St. David Street North/Highway 6, with high point elevations of 424.5mASL around the existing buildings, and a low point elevation of approximately 422.4mASL at the northeast corner of the Site. The southwest portion of the Site is sloped towards the southwest property line, with a high point elevation of 424.5mASL near the approximate center of the property, and a low point elevation of 422.6mASL along the southwest property line.

2.2 Existing Servicing

Existing servicing information within the surrounding right-of-way was obtained from the topographic survey, from plan and profile information provided by the Township of Centre Wellington, and from MTE plan and profile drawings.

2.2.1 Water

There is currently an existing 300mm diameter watermain on the far (north) side of St. David Street North/Highway 6. There is an existing 150mm diameter water service from this watermain that is extended underneath St. David Street North/Highway 6 to the property line near the northern corner of the Site.

There are two existing municipal fire hydrants located on the north side of St. David Street North/Highway 6 near the Site. One is located approximately 94m to the north of the existing driveway entrance, and one is located approximately 69m to the south of the existing driveway entrance. A flow test was performed at the aforementioned hydrants by Classic Fire and Life Safety on June 21, 2022. Refer to Table 2.1 below for a summary of the flow test results.

Table 2.1 – Results of Flow Tests

Results of Flow Tests Completed June 21, 2022 by Classic Fire & Life Safety					
Test #	Outlet Inside Diameter (in.)	Number of Outlets	Pitot Pressure (PSI)	Residual Pressure (PSI)	Flow @ Residual (gal/min)
1	n/a	n/a	n/a	46	0
2	2.5	1	20	40	751
3	2.5	2	12 + 14	38	1,209

Refer to Appendix A for further details.

2.2.2 Sanitary

There is an existing 300mm diameter municipal sanitary sewer along the far (north) side of St. David Street North/Highway 6 which drains southeast, at a depth of approximately 5.7m to 6.6m below the centreline elevation of the road. There is an existing 150mm diameter sanitary service from the Site to the 300mm diameter sewer, extended to an existing manhole near the northern corner of the Site. The depth of the 150mm diameter service at the manhole is approximately 4.8m.

2.2.3 Storm

There is an existing 500mm diameter Corrugated Metal Pipe (CMP) culvert underneath the existing driveway entrance, draining southeast in the ditch along the Site's frontage with St. David Street North/Highway 6. The culvert obvert is at a depth of approximately 1m below the existing grade of the driveway.

2.3 Existing Soils Information

A Geotechnical Investigation was completed for the Site by MTE in June 2023. Four boreholes were advanced to depths between 5.0 and 6.7m below grade. The investigation revealed the subsurface soil conditions as being generally comprised of surficial topsoil underlain by native silt and sand deposits.

Monitoring wells were installed in three of the boreholes to facilitate monitoring and measurement of groundwater elevations. Groundwater elevations measured in August 2023 were found to be between 1.7m-2.7m below grade, at elevations of 421.2 to 421.8 meters above sea level (masl). Ongoing monitoring of the groundwater levels is being completed as part of a Hydrogeological Investigation for the Site, also being completed by MTE.

The complete Geotechnical Investigation and Hydrogeological Investigations are included in the resubmission package under separate cover.

The Tile Drainage layer on OMAFRA Ag-Maps GIS mapping indicates that systematic tile drainage may be present on the southwestern half of the Site.

2.4 Reviewing Agencies

2.4.1 Township of Centre Wellington

Functional grading, servicing and stormwater management designs as well as this Functional Servicing and Stormwater Management Report will be required for submission to the Township of Centre Wellington in support of the Zoning By-Law Amendment and Vacant Land Condominium applications. The Township will also be responsible for the review and approval of site plans, site grading, servicing, stormwater management, lighting and landscape design and ultimately issuing building permits.

2.4.2 Ministry of Transportation

St. David Street North is a part of Highway 6, a provincially maintained highway. As such, the Ministry of Transportation (MTO) will be circulated on the Zoning By-Law Amendment and Site Plan Applications and will need to approve the site grading, servicing and stormwater management designs. An entrance permit will need to be obtained from the MTO for the new entrance off St. David Street North/Highway 6.

2.4.3 Grand River Conservation Authority

The Site also falls within the area regulated by the Grand River Conservation Authority (GRCA). As such, the site engineering design will also be submitted to the GRCA for review and approval.

3.0 PROPOSED GRADING AND SERVICING STRATEGY

Preliminary grading and servicing strategies have been developed based on the topographic survey, plan and profile information, and the Concept Plan provided by MHBC, dated October 2, 2023. Refer to the enclosed MTE Drawings C2.1 and C2.2 for details. These grading and servicing strategies will be further refined during detailed design during the Site Plan Approval process.

3.1 Proposed Grading

The proposed vacant land condominium development consists of 12 single-detached houses and 37 townhouse units, complete with a common element roadway and driveway entrance from St. David Street North/Highway 6. The proposed grading strategy will respect the existing grades along St. David Street North/Highway 6, and all other property boundaries. The majority of the grading internal to the Site will involve directing stormwater runoff to the existing ditch along the south side of St. David Street North/Highway 6. Stormwater runoff will be conveyed to the existing ditch via an on-site storm sewer system, and via a rear-yard swale along the southeast property line. For the units along the south end of the Site, runoff from the rear of the units will continue to drain to the southwest property line. Refer to MTE Drawing C2.1 for an illustration of the functional grading design.

3.2 Proposed Servicing

The following sections provide details regarding the preliminary proposed water, sanitary and storm servicing for the proposed development. Refer to MTE Drawing C2.2 for an illustration of the functional servicing design.

3.2.1 Water

The existing 150mm diameter water service currently extended to the northern corner of the Site will service the proposed development. At the property line, the 150mm diameter watermain will be upsized to 250mm diameter, and will be extended in the common element roadway to service each unit. Each unit will be serviced off the proposed watermain with a 25mm diameter domestic water service connection. It is anticipated that two on-site fire hydrants will also be required for the proposed development, as shown on the enclosed MTE Drawing C2.2.

Water Demand

Various guidelines and references exist for calculating the required water supply for firefighting purposes. In Ontario, there are two standards/guidelines that are most often referenced:

- Ontario Building Code (OBC) – provincial codes and guidelines published by the Ministry of Municipal Affairs and Housing for the Province of Ontario; and
- The Fire Underwriters Survey (FUS) – an insurance industry guideline.

Many municipalities in Ontario use both the OBC and the FUS fire flow requirements for assessing firefighting water supply requirements. Ideally, fire flow demands for new developments are calculated based on the FUS criteria; however, it is not always reasonable to expect that the local existing municipal infrastructure has the operational capacity to supply water at the rates prescribed in the FUS guidelines. As a result, at no time shall the available fire flow be less than that required by the Ontario Building Code.

The pressures and flows at the proposed private hydrant must be sufficient for firefighting conditions as established by the Ontario Building Code (2012). The minimum residual pressure permitted under firefighting conditions is 140.0kPa (20.3psi) per OBC 2012 A-3.2.5.7 3(b).

The buildings are proposed to be of wood frame construction (combustible construction). For the purposes of this analysis, the worst-case scenario was determined to be the future townhouse building located on Units 28-32. This building has the largest allowable footprint, and in a firefighting scenario the hydrant furthest from the connection the municipal main will be utilized. The OBC and FUS requirements were calculated for this worst-case scenario for reference and are shown in Table 3.1. Refer to Appendix A for detailed calculations.

Table 3.1 – Required Fire Flow

Building	OBC (L/s)	FUS (L/s)
Proposed Building*	4,500	17,000

• A detailed analysis will need to be completed once the final building design has been completed. Additional fire walls may be required once the final plans are developed.

For this design, pressure and flow information for the existing 300mm diameter municipal watermain in the St. David Street North/Highway 6 right-of-way was taken from the hydrant flow testing results as detailed in Section 2.2.1.

The minimum water supply flow rate for the proposed development is 283.0L/s (17,000L/min) based on the calculation method specified in the FUS. The residual pressures at the proposed hydrants are less than the minimum allowable pressure of 140kPa based on the FUS calculation method.

The minimum water supply flow rate for the proposed development is 75.0L/s (4,500L/min) based on the calculation method specified by the OBC. The residual pressure at the proposed hydrant was calculated to be 184kPa at a flow rate of 75.0L/s (4,500L/min), which is greater than the minimum allowable pressure of 140kPa per OBC 2012. Therefore, the proposed watermain configuration is expected to be sufficient. Based on a maximum day domestic demand of 0.44L/s and the fire flow demand of 75.0L/s, the total water demand for the Site is expected to be 75.4L/s.

The fire flow demand calculations completed in this report assume that the proposed buildings will have two above grade stories. Should the buildings increase to a height of 3-stories as

design progresses, fire walls may be required to meet previously described pressure and flow requirements set forth by the OBC.

3.2.2 Sanitary

A sanitary flow design sheet has been prepared to determine the flows anticipated to be generated by the proposed development. With the 12 units proposed for detached homes and 37 units proposed for townhouses, the resulting peak flow rate from the Site is expected to be 2.42L/s. Refer to Appendix A for the Sanitary Flow Design Sheet.

A 150mm diameter private sanitary sewer will be connected to the existing sanitary manhole near the northern corner of the Site, and will be extended throughout the common element area of the Site, servicing each of the proposed units.

The proposed 150mm diameter sanitary sewer has a minimum design slope of slope of 1.00%, corresponding to a full flow pipe capacity of 15.22L/s. Therefore, the proposed 150mm diameter sanitary sewer has sufficient capacity for this development.

3.2.3 Storm

A private storm sewer system is proposed along the common element roadways within the proposed development. The storm sewer system, which will include several catchbasins, manholes, and catchbasin manholes, will convey runoff from the roadways, driveways, landscaped areas, and several of the building roofs through an oil and grit separator unit (OGS) before discharging to the existing ditch along the south side of St. David Street North/Highway 6. A storm sewer design sheet for the last pipe run from the Site is included in Appendix A. The major overland flow route for the Site will be to the existing ditch along St. David Street North/Highway 6.

Specifications and details of these proposed servicing strategies will be further refined during detailed design.

4.0 PRELIMINARY STORM WATER MANAGEMENT DESIGN

4.1 SWM Criteria

In the existing condition, stormwater runoff from the northeastern end of the Site is directed to the existing ditch along St. David Street North/Highway 6. Stormwater runoff from the southwestern end of the Site is directed to the southwest property line, where it subsequently sheet flows across the adjacent property before reaching a GRCA regulated wetland, and ultimately Municipal Drain No. 1.

The stormwater management design criteria for the Site, as established by the MTO, the GRCA, and the Township of Centre Wellington, are as follows:

- i) Attenuation of the post-development peak flows for the 2-, 5-, 10-, 25-, 50-, and 100-year storm events to the pre-development (existing) peak flows;
- ii) Implementation of Enhanced (Level 1) water quality controls;
- iii) Implementation of Erosion and Sediment Control Measures; and
- iv) Provide an infiltration water balance for the entire Site area, and a surface runoff water balance for the portion of the Site draining to the wetland.

4.2 Water Quantity Control

In order to successfully complete the preliminary stormwater management design for the Site, the following specific tasks were undertaken:

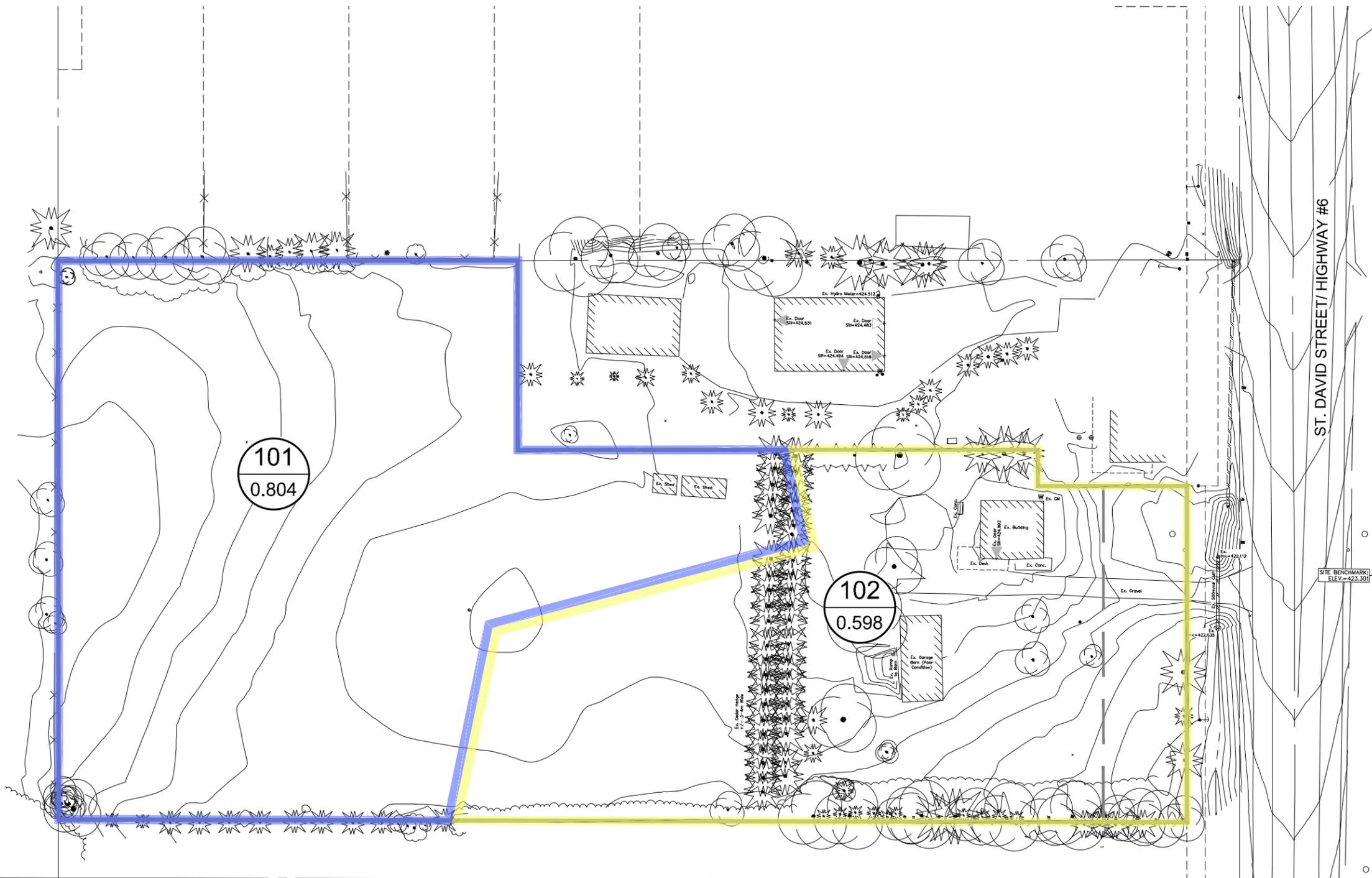
- i) Calculate the allowable runoff rates using MIDUSS NET;
- ii) Determine the percent impervious of the Site and catchment parameters for inclusion in MIDUSS NET modelling; and
- iii) Calculate post-development runoff hydrographs using MIDUSS NET.

The following table summarizes the catchments used in modelling the Site. The pre-development condition was separated into two catchment areas: the southwestern portion of the Site that drains to the southwest property line and ultimately to the wetland, and the northeastern portion of the Site that drains to St. David Street North/Highway 6. The post-development condition was separated into three catchment areas: the uncontrolled area directed to the southwest property line, the controlled area directed to St. David Street North/Highway 6, and the uncontrolled area directed to St. David Street North/Highway 6. Figure 2.0 illustrates the limits of the pre-development catchment areas. Figure 3.0 illustrates the limits of the post-development catchment areas.

Table 4.1 – Catchment Parameters

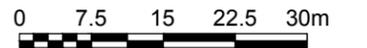
#	Catchment	Area (ha)	% Impervious	Pervious CN	Impervious CN	Slope (%)	Flow Length (m)
Pre-Development Catchment Areas							
101	Area to southwest property line, ultimately to wetland	0.804	0%	75	98	2.0	100
102	Area to Highway 6	0.598	9%	75	98	5.0	90
Post-Development Catchment Areas							
201	Uncontrolled Area to Southwest Property Line	0.136	46%	75	98	2.0	15
202	Controlled Area to Highway 6	0.962	70%	75	98	2.0	15
203	Uncontrolled Area to Highway 6	0.304	23%	75	98	2.0	120

As previously described, a geotechnical investigation was completed for the Site by MTE. Based on the underlying sand and silt soils, a pervious CN of 75 for grassed areas is appropriate.



LEGEND

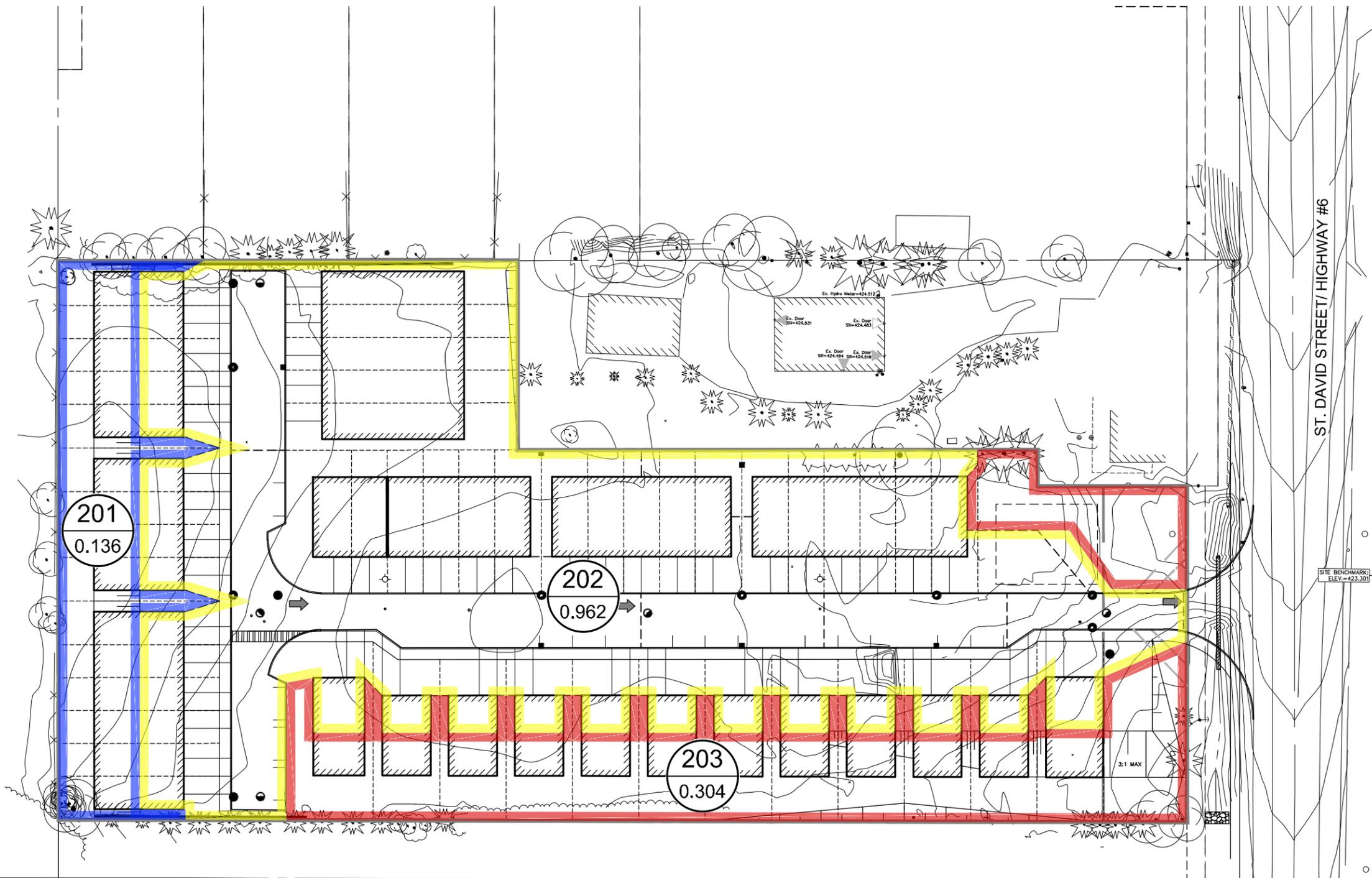
- CATCHMENT 101
- CATCHMENT 102
- 101 SUB-CATCHMENT NUMBER
- 0.804 AREA (ha.)



PROJECT
961 ST.DAVID STREET NORTH

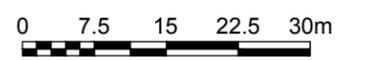
TITLE
PRE-DEVELOPMENT CATCHMENT AREAS

Drawn	JMH	Scale	1:750	Figure 2.0
Checked	NGK	Project No.	48650-100	
Date	2023-09-18	Rev No.	0	



LEGEND

- CATCHMENT 201
 - CATCHMENT 202
 - CATCHMENT 203
-
- 201 SUB-CATCHMENT NUMBER
 - 0.136 AREA (ha.)



PROJECT
961 ST.DAVID STREET NORTH

TITLE
POST-DEVELOPMENT CATCHMENT AREAS

Drawn	JMH	Scale	1:750	Figure 3.0
Checked	NGK	Project No.	48650-100	
Date	2023-09-18	Rev No.	0	

In order to achieve the stormwater requirements for the Site, runoff generated from Catchment's 201, and 203 and from the rear roofs of Catchment 202 will be directed to a 0.45m deep layer of amended topsoil in the landscaped areas of the units. The amended topsoil will allow for increased infiltration and runoff volume reduction in these catchments. Runoff generated from Catchment 202 will be conveyed to catchbasin manhole CBMH16, wherein the flow will be controlled with a 75mm orifice tube, and a 6.0m wide weir in the common element drive aisle. Storage volume will be provided by an underground storage tank, the storm sewers and structures, and by surface ponding on the surface of the common element driveway. The following table summarizes the flows generated by the Site for each storm event. The post-development flow rates are subject to change during detailed design.

Table 4.2 – Summary of Flows (MIDUSS Modelling)

Modeling Condition	Pre-Development (m ³ /s)		Post-Development (m ³ /s)	
	Area to Southwest Property Line	Area to Highway 6	Area to Southwest Property Line	Area to Highway 6
2-Year Storm Event	0.005	0.011	0.001	0.014
5-Year Storm Event	0.012	0.017	0.005	0.019
10-Year Storm Event	0.019	0.022	0.009	0.023
25-Year Storm Event	0.032	0.031	0.016	0.031
50-Year Storm Event	0.041	0.040	0.022	0.038
100-Year Storm Event	0.057	0.052	0.029	0.048

With the installation of the orifice tube, the post-development runoff from the controlled portion of the Site for the 2-, 10-, 25-, 50- and 100-year storm events is controlled to 0.012m³/s, 0.015m³/s, 0.017m³/s, 0.022m³/s, 0.022m³/s, and 0.037m³/s, respectively.

The total post-development peak flows to St. David Street North/Highway 6 exceed pre-development levels for the 2-, 5-, and 10-year storm events; however, a 75mm orifice tube is considered to be the minimum acceptable diameter, therefore additional reduction of the post-development peak flows is not considered to be feasible and the increased runoff is minimal.

The maximum ponding depth in the common element driveway is 0.17m for the 100-year storm event. As above, the ponding values are subject to change at detailed design. Please refer to Appendix B for the MIDUSS outputs.

4.3 Water Quality Control

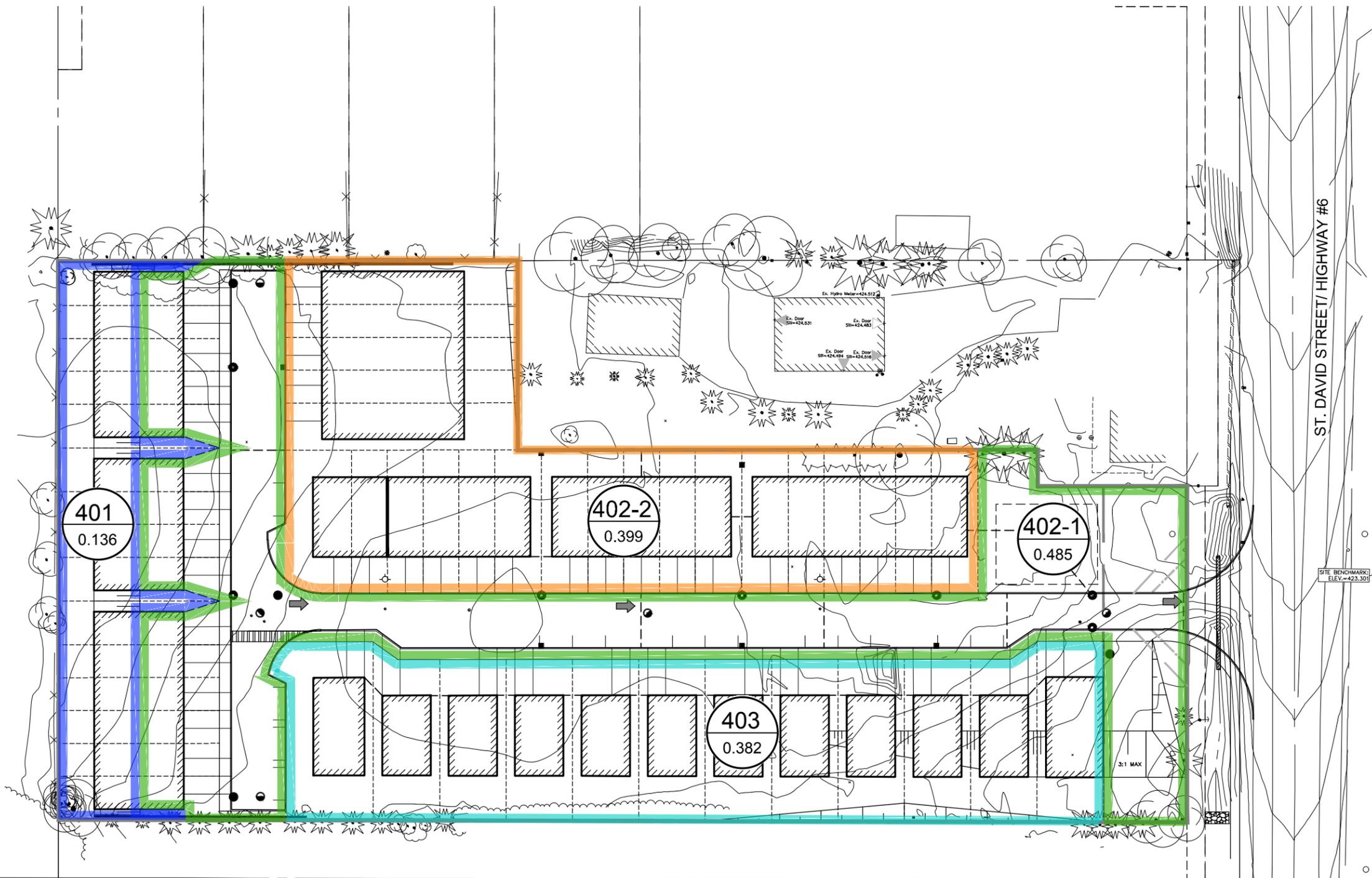
A Stormceptor Model EFO4 will be installed on the storm sewer system to provide water quality control for the Site. The chosen unit is expected to provide Enhanced (Level 1) water quality control. Refer to Appendix C for the sizing output from the Stormceptor Expert program. The Stormceptor will require regular annual maintenance to ensure it is operating properly. The owner may be required to enter into a maintenance agreement with a suitable contractor to complete this work. In addition, all the storm structures will have a 600mm sump.

4.4 Water Balance

The GRCA requires that the Site's existing hydrologic patterns related to infiltration and the wetland be maintained. As previously discussed, in the pre-development condition runoff from Catchment 101 is conveyed overland southwest across the adjacent property to a GRCA regulated wetland. Runoff from the remainder of the Site (Catchment 102) is conveyed northeast to the existing ditch on St. David Street North/Highway 6. Based on feedback from the GRCA, it is understood that infiltration inputs across the whole Site, and surface runoff inputs to the wetland are required be maintained post-development.

As previously noted, the Tile Drainage layer on OMAFRA Ag-Maps GIS mapping indicates that systematic tile drainage may be present on the southwestern half of the Site. Mapping of any tile drainage on the Site was not available at the time of publishing this report. Based on the surrounding topography and extent of the Tile Drainage layer, should any tile drainage exist on the Site, it is expected to outlet to the wetland area southwest of the Site. Although tile drainage may decrease surface runoff, it is expected that the total water yield to the wetland (lateral groundwater flow + surface runoff + tile flow) from the Site in the existing condition is not expected to be significantly different than if the Site were not systematically tiled. Therefore for the purposes of the water balance, the existing runoff, infiltration, and evapotranspiration components will be calculated based on the soil type, land cover, and topography of the Site. As groundwater monitoring continues as part of the MTE hydrogeological investigation, the impact of any existing tile drainage on groundwater levels will be assessed, particularly in relation to proposed building basements and footings.

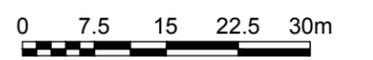
The pre-development water balance catchment areas for the Site are as per Table 4.1 and Figure 2.0. The post-development condition water balance was separated into four catchment areas: the rear roofs and yards of townhouse units along the southwest property line where runoff is conveyed to the wetland (Catchment 401); the front roofs and yards of these units, and the common element area (Catchment 402-1); the townhouse units where runoff is conveyed to Highway 6 (Catchment 402-2); and the single detached units (Catchment 403). Figure 4.0 illustrates the limits of the post-development catchment areas.



LEGEND

- CATCHMENT 401
- CATCHMENT 402-1
- CATCHMENT 402-2
- CATCHMENT 403

402-1 SUB-CATCHMENT NUMBER
 AREA (ha.)



PROJECT
961 ST.DAVID STREET NORTH

TITLE
POST-DEVELOPMENT WATER BALANCE CATCHMENT AREAS

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4.0

Canadian Climate Normal data provides an annual precipitation estimate of 945.7mm/year for the Fergus Shand Dam, which was rounded to 946mm/year for the purposes of the water balance.

To achieve the water balance requirements for the Site, a 0.45m thick layer of amended topsoil will be placed in the landscaped areas of Catchments 401, 402, and 403. Runoff from rooftop areas in these catchments will be conveyed to the amended topsoil, increasing infiltration and decreasing runoff. The following table summarizes the pre- and post-development annual surface runoff and infiltration volumes from the Site. Refer to Appendix D for detailed calculations.

Table 4.3 – Yearly Water Balance Summary

		Pre-Development	Post-Development	Volume Change	Percentage Change
Runoff Volume (m³/year)	Directed to Wetland	571	494	-77	-14%
	Directed to St. David Steet North/Highway 6	819	5,621	+4,802	-
Infiltration Volume (m³/year)	Total Site	3,869	3,961	+91	+2%

In the existing condition the annual surface runoff volume to the wetland is 571m³/year. In the post-development condition, the annual surface runoff volume decreases slightly to 494m³/year, representing a decrease of 14%. Given the relatively small pre-development runoff volume, and the grading constraints of the proposed development that limit what drainage can be directed to the southwest property line while maintaining an overland flow route to the right-of-way, the 14% decrease is considered to be within the acceptable range of a balanced condition.

The post-development surface runoff volume to St. David Street North/Highway 6 represents an increase of 4,802m³/year from the pre-development condition. An increase in runoff volume is to be expected when development occurs. As discussed in Section 4.2, there is only a minor increase in post development peak flow rates to St. David Street North/Highway 6 in the post-development condition during the 2-, 5-, and 10-year storm events. Therefore, the increase in runoff volume to the St. David Street North/Highway 6 ditch is considered to be acceptable.

In the existing condition, the annual infiltration volume from the Site is 3,869m³/year. In the post-development condition, the annual infiltration volume is 3,961m³/year, representing an increase of 2%, which is considered to be negligible.

4.5 Erosion and Sedimentation Control

Precautions will need to be taken during construction to limit erosion and sedimentation. Typically, the following measures are recommended during construction for erosion and sedimentation control:

- i) Erosion and sedimentation facilities are to be installed prior to any area grading operations;
- ii) All erosion control measures are to be inspected and monitored by the contractor and repairs are to be completed as required;
- iii) All materials and equipment used for the purpose of site preparation and project completion should be operated and stored in a manner that prevents any deleterious substance from leaving the site; and
- iv) To minimize the amount of mud being tracked onto the roadway, a mud mat should be installed at the primary construction entrance.

5.0 CONCLUSIONS

Based on the foregoing, it is concluded that:

- i) Municipal infrastructure for water and sanitary services is available along St. David Street North/Highway 6;
- ii) A fire flow analysis has been completed and demonstrates that adequate flow and pressure is available from the proposed on-site hydrants;
- iii) The water supply needs of the proposed development will not exceed what is available in the existing municipal water distribution system;
- iv) The proposed grading design will respect the natural topography of the Site to achieve a reasonable cut/fill balance where possible and match into existing grades along all property boundaries; and
- v) The SWM criteria can be satisfied with the implementation of on-site controls for water quantity and water quality.

Detailed grading and servicing designs and a detailed stormwater management design will be provided during detailed design in support of Site Plan Approval and Building Permits.

All of which is respectfully submitted,

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NGK:zeg

M:\48650\100\Reports\FSSWM\rpt_2023-11-10_FSSWM.docx

Appendix A

Design Sheets

PROJECT INFORMATION			
Project Name:	Fergus Flow Test	Const. Project #:	22-CAM-690-0568
Site Address:	961 St. David Street/Highway 6 Fergus	Design Project #:	2022-CFLS-359
City Contact:	Mike Mullen	Phone #:	519-501-7252
CFLS Contact:	Dean Wanders	Phone #:	905-514-7417
Technical Contact:	Andy Coghlin	Phone #:	519-476-0761

SITE INFORMATION

SITE MAP



Note: If the main is a dead end, the flowing hydrant shall be closest to the dead end

ITEMS TO LABEL ON MAP	HYDRANTS USED	MAIN SIZE
<input checked="" type="checkbox"/> Static / Residual & Flow Hydrants	<input checked="" type="checkbox"/> City Hydrant(s)	City: 6"
<input type="checkbox"/> Flow Direction (if the main is dead end)	<input type="checkbox"/> Site Hydrant(s)	Site:

SITE NOTES



FIRE +
LIFE
SAFETY

FLOW TEST REPORT

Form SD-003B RevDate: Nov 29, 2021

TEST INFORMATION

Minimum Required Flow:	NA	Min Ports:	2
CFLS Personnel Present:	Dean Wanders	Test Date:	2022-06-21
City / External Company:	Infrastructure Services	Test Time:	1:00pm

TEST EQUIPMENT

<input type="checkbox"/> Hose Monsters with built in Pitot	Hose length used:
<input type="checkbox"/> Hand held pitot gauge	<input checked="" type="checkbox"/> Pollard diffuser elbow with built in Pitot
<input type="checkbox"/> Other:	

TEST RESULTS

Number of Ports	Outlet Size (IN)	Discharge Coefficient	Pitot Reading (PSI)			Total Flow (GPM)	Static / Residual Pressure (PSI)
0 Ports	STATIC						46
1 Port	2.5	0.9	20			751	40
2 Ports	2.5	0.9	12	14		1,209	38
3 Ports	2.5	0.9				0	
4 Ports	2.5	0.9				0	
0 Ports	STATIC RE-CHECK						46

TEST NOTES

--

HYDRAULIC ADJUSTMENTS (FOR OFFICE USE ONLY)

ADJUSTMENTS FOR HYDRAULIC GRADE LINE (HGL)

Reservoir HGL (m):		Site Elevation (m):	
Theoretical Static Head (PSI):	0	PSI to subtract from test pressures:	46

OTHER HYDRAULIC ADJUSTMENTS

Other adjustment as required by the City / AHJ:	
---	--



**961 St. David Street
FIRE FLOW ANALYSIS**

Fergus, Ontario

Project Number: 48650-100

Date: Revised October 26, 2023

Design By: NGK

File: Q:\48650\100\Water\48650-100_Site Fire Flow Analysis with test results.xlsx

CALCULATION OF RESIDUAL PRESSURE AT ON-SITE HYDRANT

1. Boundary Conditions (Based on Fire Flow Test Results):

	Metric	Imperial	
P0 - Starting Pressure	32.35 m	46.0 psi	
P1 - Pressure at Q1	26.72 m	38.0 psi	
Q1 - From Fire Flow Test	4577 L/min	1209 U.S. gal/min	From: Hydrant Flow Test Results
Q2 - Required Flow	4500 L/min	1189 U.S. gal/min	From: Water Demand calculations by MTE
P-loss 1	5.63 m	8 psi	
P-loss 2	5.45 m	8 psi	
P2 - Residual Pressure	26.90 m	38 psi	

2. Friction Losses Through Water Service:

<i>Hazen-Williams Equation</i>			Metric	Imperial	
C _{hw} = Pipe Friction Factor			150	150	
k = conversion factor			10.675	4.727	
n = constant			1.852	1.852	
m = constant			4.8704	4.8704	
Q = Flow			4500 L/min		
Q = Flow			0.075 m ³ /s	1189 U.S. gal/min	
d = Pipe Diameter (1)			150 mm	5.91 in	
			0.15 m		
d = Pipe Diameter (2)			250 mm	9.84 in	
			0.25 m		
p = Loss/Length (1)			0.0846 m/m	0.0367 psi/ft	
p = Loss/Length (2)			0.0070 m/m	0.0030 psi/ft	
Length (1)			36 m	118 ft	Service under road & hydrant lead
Length (2)			132 m	433 ft	
Loss			3.98 m	5.7 psi	
			39 kPa		

3. Friction Losses Through Apurtenances:

Apurtenances	Number	K	Velocity m/s	Head Loss m	Total Loss m	psi
<i>Site</i>						
Valve - 150mm dia.	2	0.120	4.244	0.110	0.220	0.313
Expander - 150mm to 250mm dia.	1	2.127	4.244	1.953	1.953	2.777
45° Bend - 150mm dia.	1	0.240	4.244	0.220	0.220	0.313
45° Bend - 250mm dia.	3	0.224	1.528	0.027	0.080	0.114
250mm dia. Tee (through)	1	0.280	1.528	0.033	0.033	0.047
150mm dia. Tee (branch)	2	0.900	4.244	0.826	1.653	2.350
Total Minor Losses					4.159	5.914

4. Elevation - Elevational differences from existing hydrant to proposed hydrant

	Metric	Imperial
Elevation at Boundary (i.e. Residual Hydrant):	424.00 m	1391 ft
Elevation at Site Hydrant:	424.00 m	1391 ft
Elevation Difference = Loss/Gain	0 m	0.0 psi

ANALYSIS SUMMARY

Total Losses	8.135 m		
	79.80 kPa	11.6 psi	
Residual Pressure after Losses	18.76 m		
	184 kPa	26.7 psi	PASS
<i>Allowable Residual Pressure</i>	<i>140 kPa</i>	<i>20.3 psi</i>	

961 St. David Street
Fergus, Ontario
TOWNSHIP OF CENTRE WELLINGTON

Project Number: 48650-100
Date: October 28, 2023
Design By: NGK
Checked By: JPL
File: Q:\48650\100\Sanitary\48650-100 Sanitary Sewer Design Sheet Waterloo (SSMS) Rev7.xls

SANITARY SEWER DESIGN SHEET
ENGINEERING AND PUBLIC WORKS

Drainage Area Plan No: n/a

Design Parameters

Average Daily Flow		Mannings "n"	0.013
Residential	350.00 L/capita/day	Min. Velocity	0.6 m/sec
Commercial	1.16 L/s/ha	Max. Velocity	3.0 m/sec
Industrial	0.50 L/s/ha	Residential Harmon Peaking Factor (F) $F = 1 + 14/(4 + P^{0.5})$	
Inst. / School	0.25 L/s/ha	Commercial Peaking Factor = 2.5	
		Residential Areas Infiltration ¹	0.15 L/s/ha



LOCATION				RESIDENTIAL AREAS AND POPULATION						SCHOOL, INSTITUTIONAL			COMMERCIAL			INDUSTRIAL			INFILTRATION			DESIGN																	
STREET	AREA NO.	MANHOLE LOCATION		AREA	No. UNITS @ 3.25 PPU	No. UNITS @ 2.44 PPU	POPUL.	CUMUL POPUL.	PEAK FACTOR "F"	PEAK RES. FLOW	HECTARES AND FLOW OF EACH ZONING									TOTALS- C-I FLOW	AREA	CUMUL AREA	INFIL FLOW	TOTAL VOLUME FLOW	LENGTH	SLOPE	PIPE SIZE	CAPACITY	FULL FLOW VELOCITY										
		FROM MH	TO MH								0.25 L/s/ha			1.16 L/s/ha			0.50 L/s/ha													L/sec	ha	ha	L/sec	L/sec	m	%	mm	L/sec.	m/s
		ha	ha								L/sec	ha	ha	L/sec	ha	ha	L/sec																						
Proposed development				1.402	12.00	37.00	0.129	0.129	4.211337	2.2055										1.402	1.402	0.2103	2.4158	50.0	1.00	150	15.2217	0.862											

961 St. David Street
 Fergus, Ontario
 Township of Centre Wellington

STORM SEWER DESIGN SHEET
ENGINEERING AND PUBLIC WORKS

Design Parameters		
5 YEAR STORM		
Q=kAIC, k=0.00278	Manning's "n"	0.013
Intensity (I) = a/(tc+b) ²	Min. Velocity	0.800 m/s
a = 500	Max. Velocity	6.000 m/s
b = 0.24		
c = 0.6877		



Project Number: 48650-100
 Date: November 10, 2023
 Design By: NGK
 Checked By: JPL
 File: Q:\48650\100\Storm\Storm Sewer Design Sheet Kitchener Rev10.xlsx

Drainage Area Plan No:

LOCATION				STORMWATER FLOW							DESIGN						
STREET	AREA NUMBER	MANHOLE LOCATION		AREA (A)	RUNOFF COEFF. (C)	A x C	CUMUL. A x C	CONCENTRATION TIME		RAIN INTENSITY (I)	FLOW (Q)	PIPE SIZE	LENGTH	SLOPE	CAPACITY	FULL FLOW VELOCITY	
		FROM MH	TO MH					TOTAL	IN PIPE							mm	m
				ha	ha		ha	min	min	mm/hr	L/s	mm	m	%	L/s	m/s	%
Controlled Area				0.962				5-year flow taken from MIDUSS model			15.00000	250	10.0	0.50	42.04989	0.8566	35.67

Appendix B

MIDUSS Output

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                      2yr pre.Out"
7 "          Licensee name:                        A"
8 "          Company                               "
9 "          Date & Time last used:                10/27/2023 at 2:02:20 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          375.000 Coefficient A"
17 "          0.240  Constant B"
18 "          0.689  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          119.788  mm/hr"
23 "          Total depth                 31.396  mm"
24 "          6  002hyd  Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101  Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000  % Impervious"
31 "          0.804  Total Area"
32 "          100.000 Flow length"
33 "          2.000  Overland Slope"
34 "          0.804  Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000  Pervious slope"
37 "          0.000  Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000  Impervious slope"
40 "          0.250  Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.156  Pervious Runoff coefficient"
43 "          0.100  Pervious Ia/S coefficient"
44 "          8.467  Pervious Initial abstraction"
45 "          0.015  Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000  Impervious Runoff coefficient"
48 "          0.100  Impervious Ia/S coefficient"
49 "          0.518  Impervious Initial abstraction"
50 "          0.005  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101  Pervious  Impervious  Total Area  "
52 "          Surface Area  0.804  0.000  0.804  hectare"
53 "          Time of concentration  56.110  4.409  56.110  minutes"
54 "          Time to Centroid  181.077  97.331  181.077  minutes"
55 "          Rainfall depth  31.396  31.396  31.396  mm"
56 "          Rainfall volume  252.42  0.00  252.42  c.m"
57 "          Rainfall losses  26.511  5.151  26.511  mm"
58 "          Runoff depth  4.885  26.245  4.885  mm"
59 "          Runoff volume  39.28  0.00  39.28  c.m"
60 "          Runoff coefficient  0.156  0.000  0.156  "
61 "          Maximum flow  0.005  0.000  0.005  c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.005  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.156	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.828	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.011	0.000	0.000	0.000	c.m/sec"	
91 "	Catchment 102	Pervious	Impervious	Total Area	"	
92 "	Surface Area	0.544	0.054	0.598	hectare"	
93 "	Time of concentration	40.013	3.144	27.299	minutes"	
94 "	Time to Centroid	160.212	95.266	137.817	minutes"	
95 "	Rainfall depth	31.396	31.396	31.396	mm"	
96 "	Rainfall volume	170.85	16.90	187.75	c.m"	
97 "	Rainfall losses	26.511	5.398	24.611	mm"	
98 "	Runoff depth	4.885	25.997	6.785	mm"	
99 "	Runoff volume	26.58	13.99	40.57	c.m"	
100 "	Runoff coefficient	0.156	0.828	0.216	"	
101 "	Maximum flow	0.004	0.010	0.011	c.m/sec"	
102 "	38	START/RE-START TOTALS "				
103 "	3	Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000	hectare"	
105 "		Total Impervious area		0.000	hectare"	
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                      5yr pre.Out"
7 "          Licensee name:                          A"
8 "          Company                                "
9 "          Date & Time last used:                10/27/2023 at 2:01:23 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          500.000 Coefficient A"
17 "          0.240  Constant B"
18 "          0.688  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          160.061  mm/hr"
23 "          Total depth                42.145  mm"
24 "          6  005hyd Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101 Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000 % Impervious"
31 "          0.804 Total Area"
32 "          100.000 Flow length"
33 "          2.000 Overland Slope"
34 "          0.804 Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000 Pervious slope"
37 "          0.000 Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000 Impervious slope"
40 "          0.250 Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.227 Pervious Runoff coefficient"
43 "          0.100 Pervious Ia/S coefficient"
44 "          8.467 Pervious Initial abstraction"
45 "          0.015 Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000 Impervious Runoff coefficient"
48 "          0.100 Impervious Ia/S coefficient"
49 "          0.518 Impervious Initial abstraction"
50 "          0.012  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101 Pervious Impervious Total Area "
52 "          Surface Area 0.804 0.000 0.804 hectare"
53 "          Time of concentration 39.662 3.873 39.662 minutes"
54 "          Time to Centroid 160.316 95.565 160.316 minutes"
55 "          Rainfall depth 42.145 42.145 42.145 mm"
56 "          Rainfall volume 338.84 0.00 338.84 c.m"
57 "          Rainfall losses 32.561 5.881 32.561 mm"
58 "          Runoff depth 9.583 36.263 9.583 mm"
59 "          Runoff volume 77.05 0.00 77.05 c.m"
60 "          Runoff coefficient 0.227 0.000 0.227 "
61 "          Maximum flow 0.012 0.000 0.012 c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.012  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.227	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.869	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.017	0.000	0.000	0.000	0.000	c.m/sec"
91 "	Catchment 102	Pervious	Impervious	Total Area		"
92 "	Surface Area	0.544	0.054	0.598		hectare"
93 "	Time of concentration	28.284	2.762	21.277		minutes"
94 "	Time to Centroid	144.474	93.560	130.497		minutes"
95 "	Rainfall depth	42.145	42.145	42.145		mm"
96 "	Rainfall volume	229.34	22.68	252.02		c.m"
97 "	Rainfall losses	32.570	5.508	30.134		mm"
98 "	Runoff depth	9.575	36.636	12.011		mm"
99 "	Runoff volume	52.11	19.72	71.82		c.m"
100 "	Runoff coefficient	0.227	0.869	0.285		"
101 "	Maximum flow	0.011	0.015	0.017		c.m/sec"
102 "	38	START/RE-START TOTALS				"
103 "		3 Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000		hectare"
105 "		Total Impervious area		0.000		hectare"
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     10yr pre.Out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:              10/27/2023 at 2:00:18 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          595.000 Coefficient A"
17 "          0.360  Constant B"
18 "          0.691  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          186.431  mm/hr"
23 "          Total depth                49.226  mm"
24 "          6  010hyd  Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101  Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000  % Impervious"
31 "          0.804  Total Area"
32 "          100.000 Flow length"
33 "          2.000  Overland Slope"
34 "          0.804  Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000  Pervious slope"
37 "          0.000  Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000  Impervious slope"
40 "          0.250  Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.269  Pervious Runoff coefficient"
43 "          0.100  Pervious Ia/S coefficient"
44 "          8.467  Pervious Initial abstraction"
45 "          0.015  Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000  Impervious Runoff coefficient"
48 "          0.100  Impervious Ia/S coefficient"
49 "          0.518  Impervious Initial abstraction"
50 "          0.019  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101  Pervious  Impervious  Total Area  "
52 "          Surface Area  0.804  0.000  0.804  hectare"
53 "          Time of concentration  34.073  3.625  34.073  minutes"
54 "          Time to Centroid  151.986  94.644  151.986  minutes"
55 "          Rainfall depth  49.226  49.226  49.226  mm"
56 "          Rainfall volume  395.78  0.00  395.78  c.m"
57 "          Rainfall losses  35.986  6.385  35.986  mm"
58 "          Runoff depth  13.240  42.841  13.240  mm"
59 "          Runoff volume  106.45  0.00  106.45  c.m"
60 "          Runoff coefficient  0.269  0.000  0.269  "
61 "          Maximum flow  0.019  0.000  0.019  c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.019  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.269	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.886	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.022	0.000	0.000	0.000	0.000	c.m/sec"
91 "	Catchment 102	Pervious	Impervious	Total Area		"
92 "	Surface Area	0.544	0.054	0.598		hectare"
93 "	Time of concentration	24.298	2.585	18.962		minutes"
94 "	Time to Centroid	138.081	92.658	126.916		minutes"
95 "	Rainfall depth	49.226	49.226	49.226		mm"
96 "	Rainfall volume	267.88	26.49	294.37		c.m"
97 "	Rainfall losses	35.985	5.594	33.249		mm"
98 "	Runoff depth	13.241	43.632	15.977		mm"
99 "	Runoff volume	72.06	23.48	95.54		c.m"
100 "	Runoff coefficient	0.269	0.886	0.325		"
101 "	Maximum flow	0.018	0.018	0.022		c.m/sec"
102 "	38	START/RE-START TOTALS				"
103 "	3	Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000		hectare"
105 "		Total Impervious area		0.000		hectare"
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                        Q:\48650\100\SWM"
6 "          Output filename:                    25yr pre.Out"
7 "          Licensee name:                      A"
8 "          Company                            "
9 "          Date & Time last used:             10/27/2023 at 1:58:22 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          702.000 Coefficient A"
17 "          0.350  Constant B"
18 "          0.690  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          220.574  mm/hr"
23 "          Total depth                58.353  mm"
24 "          6  025hyd  Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101  Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000  % Impervious"
31 "          0.804  Total Area"
32 "          100.000 Flow length"
33 "          2.000  Overland Slope"
34 "          0.804  Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000  Pervious slope"
37 "          0.000  Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000  Impervious slope"
40 "          0.250  Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.317  Pervious Runoff coefficient"
43 "          0.100  Pervious Ia/S coefficient"
44 "          8.467  Pervious Initial abstraction"
45 "          0.015  Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000  Impervious Runoff coefficient"
48 "          0.100  Impervious Ia/S coefficient"
49 "          0.518  Impervious Initial abstraction"
50 "          0.032  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101  Pervious  Impervious  Total Area  "
52 "          Surface Area  0.804  0.000  0.804  hectare"
53 "          Time of concentration  29.275  3.375  29.275  minutes"
54 "          Time to Centroid  144.683  93.660  144.683  minutes"
55 "          Rainfall depth  58.353  58.353  58.353  mm"
56 "          Rainfall volume  469.16  0.00  469.16  c.m"
57 "          Rainfall losses  39.869  6.386  39.869  mm"
58 "          Runoff depth  18.484  51.966  18.484  mm"
59 "          Runoff volume  148.61  0.00  148.61  c.m"
60 "          Runoff coefficient  0.317  0.000  0.317  "
61 "          Maximum flow  0.032  0.000  0.032  c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.032  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.317	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.902	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.031	0.000	0.000	0.000	0.000	c.m/sec"
91 "	Catchment 102	Pervious	Impervious	Total Area		"
92 "	Surface Area	0.544	0.054	0.598		hectare"
93 "	Time of concentration	20.876	2.407	16.818		minutes"
94 "	Time to Centroid	132.461	91.887	123.546		minutes"
95 "	Rainfall depth	58.353	58.353	58.353		mm"
96 "	Rainfall volume	317.54	31.41	348.95		c.m"
97 "	Rainfall losses	39.869	5.725	36.796		mm"
98 "	Runoff depth	18.484	52.628	21.557		mm"
99 "	Runoff volume	100.58	28.32	128.91		c.m"
100 "	Runoff coefficient	0.317	0.902	0.369		"
101 "	Maximum flow	0.028	0.022	0.031		c.m/sec"
102 "	38	START/RE-START TOTALS				"
103 "	3	Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000		hectare"
105 "		Total Impervious area		0.000		hectare"
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                      50yr pre.Out"
7 "          Licensee name:                        A"
8 "          Company                               "
9 "          Date & Time last used:                10/27/2023 at 1:59:30 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          780.000 Coefficient A"
17 "          0.360  Constant B"
18 "          0.690  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          244.972  mm/hr"
23 "          Total depth                 65.003  mm"
24 "          6  050hyd  Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101  Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000  % Impervious"
31 "          0.804  Total Area"
32 "          100.000 Flow length"
33 "          2.000  Overland Slope"
34 "          0.804  Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000  Pervious slope"
37 "          0.000  Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000  Impervious slope"
40 "          0.250  Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.348  Pervious Runoff coefficient"
43 "          0.100  Pervious Ia/S coefficient"
44 "          8.467  Pervious Initial abstraction"
45 "          0.015  Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000  Impervious Runoff coefficient"
48 "          0.100  Impervious Ia/S coefficient"
49 "          0.518  Impervious Initial abstraction"
50 "          0.041  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101  Pervious  Impervious  Total Area  "
52 "          Surface Area  0.804  0.000  0.804  hectare"
53 "          Time of concentration  26.777  3.229  26.777  minutes"
54 "          Time to Centroid  140.702  93.078  140.702  minutes"
55 "          Rainfall depth  65.003  65.003  65.003  mm"
56 "          Rainfall volume  522.62  0.00  522.62  c.m"
57 "          Rainfall losses  42.373  6.372  42.373  mm"
58 "          Runoff depth  22.629  58.631  22.629  mm"
59 "          Runoff volume  181.94  0.00  181.94  c.m"
60 "          Runoff coefficient  0.348  0.000  0.348  "
61 "          Maximum flow  0.041  0.000  0.041  c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.041  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.347	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.910	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.040	0.000	0.000	0.000	0.000	c.m/sec"
91 "	Catchment 102	Pervious	Impervious	Total Area		"
92 "	Surface Area	0.544	0.054	0.598		hectare"
93 "	Time of concentration	19.095	2.302	15.639		minutes"
94 "	Time to Centroid	129.423	91.468	121.612		minutes"
95 "	Rainfall depth	65.003	65.003	65.003		mm"
96 "	Rainfall volume	353.73	34.98	388.72		c.m"
97 "	Rainfall losses	42.415	5.826	39.122		mm"
98 "	Runoff depth	22.587	59.176	25.880		mm"
99 "	Runoff volume	122.92	31.85	154.76		c.m"
100 "	Runoff coefficient	0.347	0.910	0.398		"
101 "	Maximum flow	0.036	0.025	0.040		c.m/sec"
102 "	38	START/RE-START TOTALS				"
103 "		3 Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000		hectare"
105 "		Total Impervious area		0.000		hectare"
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

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1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     100yr pre.Out"
7 "          Licensee name:                       A"
8 "          Company                               "
9 "          Date & Time last used:               10/27/2023 at 3:55:18 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          851.000 Coefficient A"
17 "          0.290  Constant B"
18 "          0.687  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          270.786  mm/hr"
23 "          Total depth                 71.828  mm"
24 "          6  100hyd  Hydrograph extension used in this file"
25 " 33      CATCHMENT 101"
26 "          1  Triangular SCS"
27 "          1  Equal length"
28 "          1  SCS method"
29 "          101  Area to southwest property line, ultimately to Mun. Drain #1"
30 "          0.000  % Impervious"
31 "          0.804  Total Area"
32 "          100.000 Flow length"
33 "          2.000  Overland Slope"
34 "          0.804  Pervious Area"
35 "          100.000 Pervious length"
36 "          2.000  Pervious slope"
37 "          0.000  Impervious Area"
38 "          100.000 Impervious length"
39 "          2.000  Impervious slope"
40 "          0.250  Pervious Manning 'n'"
41 "          75.000 Pervious SCS Curve No."
42 "          0.377  Pervious Runoff coefficient"
43 "          0.100  Pervious Ia/S coefficient"
44 "          8.467  Pervious Initial abstraction"
45 "          0.015  Impervious Manning 'n'"
46 "          98.000 Impervious SCS Curve No."
47 "          0.000  Impervious Runoff coefficient"
48 "          0.100  Impervious Ia/S coefficient"
49 "          0.518  Impervious Initial abstraction"
50 "          0.056  0.000  0.000  0.000 c.m/sec"
51 "          Catchment 101  Pervious  Impervious  Total Area  "
52 "          Surface Area  0.804  0.000  0.804  hectare"
53 "          Time of concentration  24.716  3.096  24.715  minutes"
54 "          Time to Centroid  137.449  92.639  137.449  minutes"
55 "          Rainfall depth  71.828  71.828  71.828  mm"
56 "          Rainfall volume  577.50  0.00  577.50  c.m"
57 "          Rainfall losses  44.722  6.351  44.722  mm"
58 "          Runoff depth  27.106  65.478  27.106  mm"
59 "          Runoff volume  217.93  0.00  217.93  c.m"
60 "          Runoff coefficient  0.377  0.000  0.377  "
61 "          Maximum flow  0.056  0.000  0.056  c.m/sec"
62 " 40      HYDROGRAPH Start - New Tributary"
63 "          2  Start - New Tributary"
64 "          0.056  0.000  0.000  0.000"
65 " 33      CATCHMENT 102"
66 "          1  Triangular SCS"
67 "          1  Equal length"
68 "          1  SCS method"
    
```

69 "	102	Area to Highway 6"				
70 "	9.000	% Impervious"				
71 "	0.598	Total Area"				
72 "	90.000	Flow length"				
73 "	5.000	Overland Slope"				
74 "	0.544	Pervious Area"				
75 "	90.000	Pervious length"				
76 "	5.000	Pervious slope"				
77 "	0.054	Impervious Area"				
78 "	90.000	Impervious length"				
79 "	5.000	Impervious slope"				
80 "	0.250	Pervious Manning 'n'"				
81 "	75.000	Pervious SCS Curve No."				
82 "	0.377	Pervious Runoff coefficient"				
83 "	0.100	Pervious Ia/S coefficient"				
84 "	8.467	Pervious Initial abstraction"				
85 "	0.015	Impervious Manning 'n'"				
86 "	98.000	Impervious SCS Curve No."				
87 "	0.917	Impervious Runoff coefficient"				
88 "	0.100	Impervious Ia/S coefficient"				
89 "	0.518	Impervious Initial abstraction"				
90 "	0.052	0.000	0.000	0.000	0.000	c.m/sec"
91 "	Catchment 102	Pervious	Impervious	Total Area		"
92 "	Surface Area	0.544	0.054	0.598		hectare"
93 "	Time of concentration	17.625	2.208	14.639		minutes"
94 "	Time to Centroid	126.874	91.122	119.949		minutes"
95 "	Rainfall depth	71.828	71.828	71.828		mm"
96 "	Rainfall volume	390.88	38.66	429.53		c.m"
97 "	Rainfall losses	44.716	5.977	41.230		mm"
98 "	Runoff depth	27.112	65.851	30.599		mm"
99 "	Runoff volume	147.54	35.44	182.98		c.m"
100 "	Runoff coefficient	0.377	0.917	0.426		"
101 "	Maximum flow	0.045	0.028	0.052		c.m/sec"
102 "	38	START/RE-START TOTALS				"
103 "	3	Runoff Totals on EXIT"				
104 "		Total Catchment area		0.000		hectare"
105 "		Total Impervious area		0.000		hectare"
106 "		Total % impervious		0.000"		
107 "	19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     2yr post r4.out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:               10/27/2023 at 4:01:22 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          375.000 Coefficient A"
17 "          0.240  Constant B"
18 "          0.689  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          119.788  mm/hr"
23 "          Total depth                 31.396  mm"
24 "          6  002hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000  % Impervious"
35 "          0.136  Total Area"
36 "          15.000  Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000  Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000  Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000  Pervious SCS Curve No."
46 "          0.043  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981  Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000  Impervious SCS Curve No."
51 "          0.248  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999  Impervious Initial abstraction"
54 "          0.001  0.000  0.000  0.000 c.m/sec"
55 "          Catchment 201  Pervious  Impervious Total Area "
56 "          Surface Area          0.073  0.063  0.136  hectare"
57 "          Time of concentration  52.330  4.179  12.363  minutes"
58 "          Time to Centroid       172.140  128.081  135.570  minutes"
59 "          Rainfall depth         31.396  31.396  31.396  mm"
60 "          Rainfall volume        23.06  19.64  42.70  c.m"
61 "          Rainfall losses        30.040  23.624  27.089  mm"
62 "          Runoff depth           1.356  7.771  4.307  mm"
63 "          Runoff volume           1.00  4.86  5.86  c.m"
64 "          Runoff coefficient      0.043  0.248  0.137  "
65 "          Maximum flow           0.000  0.001  0.001  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.001  0.000  0.000  0.000"
    
```

```

69 " 81      ADD COMMENT=====
70 "          2 Lines of comment"
71 "          IA increased to 20mm to account for roof and landscape area "
72 "          runoff reduction due to amended topsoil"
73 " 33      CATCHMENT 202"
74 "          1 Triangular SCS"
75 "          1 Equal length"
76 "          1 SCS method"
77 "          202 Controlled area to Highway 6"
78 "          70.000 % Impervious"
79 "          0.962 Total Area"
80 "          15.000 Flow length"
81 "          2.000 Overland Slope"
82 "          0.289 Pervious Area"
83 "          15.000 Pervious length"
84 "          2.000 Pervious slope"
85 "          0.673 Impervious Area"
86 "          15.000 Impervious length"
87 "          2.000 Impervious slope"
88 "          0.250 Pervious Manning 'n'"
89 "          75.000 Pervious SCS Curve No."
90 "          0.043 Pervious Runoff coefficient"
91 "          0.236 Pervious Ia/S coefficient"
92 "          19.981 Pervious Initial abstraction"
93 "          0.015 Impervious Manning 'n'"
94 "          98.000 Impervious SCS Curve No."
95 "          0.825 Impervious Runoff coefficient"
96 "          0.100 Impervious Ia/S coefficient"
97 "          0.518 Impervious Initial abstraction"
98 "          0.159 0.000 0.000 0.000 c.m/sec"
99 "          Catchment 202 Pervious Impervious Total Area "
100 "          Surface Area 0.289 0.673 0.962 hectare"
101 "          Time of concentration 52.330 1.412 2.530 minutes"
102 "          Time to Centroid 172.140 92.372 94.123 minutes"
103 "          Rainfall depth 31.396 31.396 31.396 mm"
104 "          Rainfall volume 90.61 211.42 302.03 c.m"
105 "          Rainfall losses 30.040 5.505 12.866 mm"
106 "          Runoff depth 1.356 25.891 18.530 mm"
107 "          Runoff volume 3.91 174.35 178.26 c.m"
108 "          Runoff coefficient 0.043 0.825 0.590 "
109 "          Maximum flow 0.001 0.159 0.159 c.m/sec"
110 " 40      HYDROGRAPH Add Runoff "
111 "          4 Add Runoff "
112 "          0.159 0.159 0.000 0.000"
113 " 54      POND DESIGN"
114 "          0.159 Current peak flow c.m/sec"
115 "          0.207 Target outflow c.m/sec"
116 "          178.3 Hydrograph volume c.m"
117 "          9. Number of stages"
118 "          421.990 Minimum water level metre"
119 "          424.030 Maximum water level metre"
120 "          421.990 Starting water level metre"
121 "          0 Keep Design Data: 1 = True; 0 = False"
122 "          Level Discharge Volume"
123 "          421.990 0.000 0.000"
124 "          422.200 0.00642 1.01E-05"
125 "          422.600 0.01201 85.000"
126 "          423.000 0.01572 170.000"
127 "          423.500 0.01939 211.987"
128 "          423.830 0.02147 221.426"
129 "          423.930 0.02206 239.726"
130 "          423.980 0.02235 270.251"
131 "          424.030 0.06480 325.201"
132 "          1. WEIRS"
133 "          Crest Weir Crest Left Right"
134 "          elevation coefficie breadth sideslope sideslope"
135 "          423.980 0.900 0.600 50.000 50.000"
136 "          1. ORIFICES"
    
```

137 "		Orifice	Orifice	Orifice	Number of	
138 "		invert	coefficie	diameter	orifices"	
139 "		421.990	0.820	0.0750	1.000"	
140 "		Peak outflow		0.012	c.m/sec"	
141 "		Maximum level		422.646	metre"	
142 "		Maximum storage		94.734	c.m"	
143 "		Centroidal lag		3.033	hours"	
144 "		0.159	0.159	0.012	0.000	c.m/sec"
145 " 40		HYDROGRAPH	Combine	1"		
146 "	6	Combine "				
147 "	1	Node #"				
148 "		Total to Highway #6"				
149 "		Maximum flow		0.012	c.m/sec"	
150 "		Hydrograph volume		178.968	c.m"	
151 "		0.159	0.159	0.012	0.012"	
152 " 40		HYDROGRAPH Start - New Tributary"				
153 "	2	Start - New Tributary"				
154 "		0.159	0.000	0.012	0.012"	
155 " 81		ADD COMMENT=====				
156 "	2	Lines of comment"				
157 "		IA increased to 20mm to account for roof and landscape area "				
158 "		runoff reduction due to amended topsoil"				
159 " 33		CATCHMENT 203"				
160 "	1	Triangular SCS"				
161 "	1	Equal length"				
162 "	1	SCS method"				
163 "	203	Uncontrolled to Highway 6"				
164 "	23.000	% Impervious"				
165 "	0.304	Total Area"				
166 "	120.000	Flow length"				
167 "	2.000	Overland Slope"				
168 "	0.234	Pervious Area"				
169 "	120.000	Pervious length"				
170 "	2.000	Pervious slope"				
171 "	0.070	Impervious Area"				
172 "	120.000	Impervious length"				
173 "	2.000	Impervious slope"				
174 "	0.250	Pervious Manning 'n'"				
175 "	75.000	Pervious SCS Curve No."				
176 "	0.043	Pervious Runoff coefficient"				
177 "	0.236	Pervious Ia/S coefficient"				
178 "	19.981	Pervious Initial abstraction"				
179 "	0.015	Impervious Manning 'n'"				
180 "	98.000	Impervious SCS Curve No."				
181 "	0.249	Impervious Runoff coefficient"				
182 "	3.858	Impervious Ia/S coefficient"				
183 "	19.999	Impervious Initial abstraction"				
184 "		0.001	0.000	0.012	0.012	c.m/sec"
185 "		Catchment 203	Pervious	Impervious	Total Area	"
186 "		Surface Area	0.234	0.070	0.304	hectare"
187 "		Time of concentration	182.223	14.553	76.159	minutes"
188 "		Time to Centroid	271.867	137.008	186.559	minutes"
189 "		Rainfall depth	31.396	31.396	31.396	mm"
190 "		Rainfall volume	73.49	21.95	95.44	c.m"
191 "		Rainfall losses	30.040	23.580	28.554	mm"
192 "		Runoff depth	1.356	7.816	2.842	mm"
193 "		Runoff volume	3.17	5.46	8.64	c.m"
194 "		Runoff coefficient	0.043	0.249	0.091	"
195 "		Maximum flow	0.000	0.001	0.001	c.m/sec"
196 " 40		HYDROGRAPH Add Runoff "				
197 "	4	Add Runoff "				
198 "		0.001	0.001	0.012	0.012"	
199 " 40		HYDROGRAPH Copy to Outflow"				
200 "	8	Copy to Outflow"				
201 "		0.001	0.001	0.001	0.012"	
202 " 40		HYDROGRAPH	Combine	1"		
203 "	6	Combine "				
204 "	1	Node #"				

205 "	Total to Highway #6"				
206 "	Maximum flow		0.014	c.m/sec"	
207 "	Hydrograph volume		187.607	c.m"	
208 "	0.001 0.001		0.001	0.014"	
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area		1.266	hectare"	
212 "	Total Impervious area		0.743	hectare"	
213 "	Total % impervious		58.714"		
214 " 19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     5yr post r4.out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:               10/27/2023 at 4:00:16 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          500.000 Coefficient A"
17 "          0.240  Constant B"
18 "          0.688  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          160.061  mm/hr"
23 "          Total depth                 42.145  mm"
24 "          6  005hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000 % Impervious"
35 "          0.136  Total Area"
36 "          15.000 Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000 Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000 Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000 Pervious SCS Curve No."
46 "          0.109  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981 Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000 Impervious SCS Curve No."
51 "          0.417  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999 Impervious Initial abstraction"
54 "          0.005  0.000  0.000  0.000 c.m/sec"
55 "          Catchment 201  Pervious  Impervious Total Area "
56 "          Surface Area      0.073  0.063  0.136  hectare"
57 "          Time of concentration 26.171  2.385  7.965  minutes"
58 "          Time to Centroid    143.656  111.673  119.176  minutes"
59 "          Rainfall depth     42.145  42.145  42.145  mm"
60 "          Rainfall volume    30.95  26.37  57.32  c.m"
61 "          Rainfall losses    37.551  24.551  31.571  mm"
62 "          Runoff depth        4.593  17.594  10.574  mm"
63 "          Runoff volume       3.37  11.01  14.38  c.m"
64 "          Runoff coefficient  0.109  0.417  0.251  "
65 "          Maximum flow       0.001  0.005  0.005  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.005  0.000  0.000  0.000"
    
```

```

69 " 81          ADD COMMENT=====
70 "          2 Lines of comment"
71 "          IA increased to 20mm to account for roof and landscape area "
72 "          runoff reduction due to amended topsoil"
73 " 33          CATCHMENT 202"
74 "          1 Triangular SCS"
75 "          1 Equal length"
76 "          1 SCS method"
77 "          202 Controlled area to Highway 6"
78 "          70.000 % Impervious"
79 "          0.962 Total Area"
80 "          15.000 Flow length"
81 "          2.000 Overland Slope"
82 "          0.289 Pervious Area"
83 "          15.000 Pervious length"
84 "          2.000 Pervious slope"
85 "          0.673 Impervious Area"
86 "          15.000 Impervious length"
87 "          2.000 Impervious slope"
88 "          0.250 Pervious Manning 'n'"
89 "          75.000 Pervious SCS Curve No."
90 "          0.109 Pervious Runoff coefficient"
91 "          0.236 Pervious Ia/S coefficient"
92 "          19.981 Pervious Initial abstraction"
93 "          0.015 Impervious Manning 'n'"
94 "          98.000 Impervious SCS Curve No."
95 "          0.855 Impervious Runoff coefficient"
96 "          0.100 Impervious Ia/S coefficient"
97 "          0.518 Impervious Initial abstraction"
98 "          0.226 0.000 0.000 0.000 c.m/sec"
99 "          Catchment 202 Pervious Impervious Total Area "
100 "          Surface Area 0.289 0.673 0.962 hectare"
101 "          Time of concentration 26.171 1.241 2.533 minutes"
102 "          Time to Centroid 143.656 91.016 93.743 minutes"
103 "          Rainfall depth 42.145 42.145 42.145 mm"
104 "          Rainfall volume 121.63 283.80 405.43 c.m"
105 "          Rainfall losses 37.551 6.117 15.548 mm"
106 "          Runoff depth 4.593 36.027 26.597 mm"
107 "          Runoff volume 13.26 242.61 255.86 c.m"
108 "          Runoff coefficient 0.109 0.855 0.631 "
109 "          Maximum flow 0.002 0.226 0.226 c.m/sec"
110 " 40          HYDROGRAPH Add Runoff "
111 "          4 Add Runoff "
112 "          0.226 0.226 0.000 0.000"
113 " 54          POND DESIGN"
114 "          0.226 Current peak flow c.m/sec"
115 "          0.207 Target outflow c.m/sec"
116 "          255.9 Hydrograph volume c.m"
117 "          9. Number of stages"
118 "          421.990 Minimum water level metre"
119 "          424.030 Maximum water level metre"
120 "          421.990 Starting water level metre"
121 "          0 Keep Design Data: 1 = True; 0 = False"
122 "          Level Discharge Volume"
123 "          421.990 0.000 0.000"
124 "          422.200 0.00642 1.01E-05"
125 "          422.600 0.01201 85.000"
126 "          423.000 0.01572 170.000"
127 "          423.500 0.01939 211.987"
128 "          423.830 0.02147 221.426"
129 "          423.930 0.02206 239.726"
130 "          423.980 0.02235 270.251"
131 "          424.030 0.06480 325.201"
132 "          1. WEIRS"
133 "          Crest Weir Crest Left Right"
134 "          elevation coefficie breadth sideslope sideslope"
135 "          423.980 0.900 0.600 50.000 50.000"
136 "          1. ORIFICES"
    
```

```

137 "           Orifice Orifice Orifice Number of"
138 "           invert coefficie diameter orifices"
139 "           421.990 0.820 0.0750 1.000"
140 "           Peak outflow 0.015 c.m/sec"
141 "           Maximum level 422.894 metre"
142 "           Maximum storage 147.562 c.m"
143 "           Centroidal lag 3.478 hours"
144 "           0.226 0.226 0.015 0.000 c.m/sec"
145 " 40 HYDROGRAPH Combine 1"
146 " 6 Combine "
147 " 1 Node #"
148 "           Total to Highway #6"
149 "           Maximum flow 0.015 c.m/sec"
150 "           Hydrograph volume 254.889 c.m"
151 "           0.226 0.226 0.015 0.015"
152 " 40 HYDROGRAPH Start - New Tributary"
153 " 2 Start - New Tributary"
154 "           0.226 0.000 0.015 0.015"
155 " 81 ADD COMMENT=====
156 " 2 Lines of comment"
157 "           IA increased to 20mm to account for roof and landscape area "
158 "           runoff reduction due to amended topsoil"
159 " 33 CATCHMENT 203"
160 " 1 Triangular SCS"
161 " 1 Equal length"
162 " 1 SCS method"
163 " 203 Uncontrolled to Highway 6"
164 " 23.000 % Impervious"
165 " 0.304 Total Area"
166 " 120.000 Flow length"
167 " 2.000 Overland Slope"
168 " 0.234 Pervious Area"
169 " 120.000 Pervious length"
170 " 2.000 Pervious slope"
171 " 0.070 Impervious Area"
172 " 120.000 Impervious length"
173 " 2.000 Impervious slope"
174 " 0.250 Pervious Manning 'n'"
175 " 75.000 Pervious SCS Curve No."
176 " 0.109 Pervious Runoff coefficient"
177 " 0.236 Pervious Ia/S coefficient"
178 " 19.981 Pervious Initial abstraction"
179 " 0.015 Impervious Manning 'n'"
180 " 98.000 Impervious SCS Curve No."
181 " 0.424 Impervious Runoff coefficient"
182 " 3.858 Impervious Ia/S coefficient"
183 " 19.999 Impervious Initial abstraction"
184 "           0.005 0.000 0.015 0.015 c.m/sec"
185 "           Catchment 203 Pervious Impervious Total Area "
186 "           Surface Area 0.234 0.070 0.304 hectare"
187 "           Time of concentration 91.133 8.304 46.625 minutes"
188 "           Time to Centroid 205.843 118.191 158.743 minutes"
189 "           Rainfall depth 42.145 42.145 42.145 mm"
190 "           Rainfall volume 98.65 29.47 128.12 c.m"
191 "           Rainfall losses 37.547 24.268 34.493 mm"
192 "           Runoff depth 4.598 17.877 7.652 mm"
193 "           Runoff volume 10.76 12.50 23.26 c.m"
194 "           Runoff coefficient 0.109 0.424 0.182 "
195 "           Maximum flow 0.001 0.005 0.005 c.m/sec"
196 " 40 HYDROGRAPH Add Runoff "
197 " 4 Add Runoff "
198 "           0.005 0.005 0.015 0.015"
199 " 40 HYDROGRAPH Copy to Outflow"
200 " 8 Copy to Outflow"
201 "           0.005 0.005 0.005 0.015"
202 " 40 HYDROGRAPH Combine 1"
203 " 6 Combine "
204 " 1 Node #"
    
```

205 "	Total to Highway #6"				
206 "	Maximum flow		0.019	c.m/sec"	
207 "	Hydrograph volume		278.150	c.m"	
208 "	0.005 0.005		0.005	0.019"	
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area		1.266	hectare"	
212 "	Total Impervious area		0.743	hectare"	
213 "	Total % impervious		58.714"		
214 " 19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     10yr post r4.out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:               10/27/2023 at 3:59:18 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          595.000 Coefficient A"
17 "          0.360  Constant B"
18 "          0.691  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          186.431  mm/hr"
23 "          Total depth                49.226  mm"
24 "          6  010hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000  % Impervious"
35 "          0.136  Total Area"
36 "          15.000  Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000  Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000  Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000  Pervious SCS Curve No."
46 "          0.152  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981  Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000  Impervious SCS Curve No."
51 "          0.495  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999  Impervious Initial abstraction"
54 "          0.009  0.000  0.000  0.000  c.m/sec"
55 "          Catchment 201  Pervious  Impervious  Total Area  "
56 "          Surface Area          0.073  0.063  0.136  hectare"
57 "          Time of concentration  19.542  1.701  6.436  minutes"
58 "          Time to Centroid       134.145  106.408  113.769  minutes"
59 "          Rainfall depth         49.226  49.226  49.226  mm"
60 "          Rainfall volume        36.15  30.80  66.95  c.m"
61 "          Rainfall losses        41.729  24.869  33.973  mm"
62 "          Runoff depth            7.497  24.357  15.253  mm"
63 "          Runoff volume           5.51  15.24  20.74  c.m"
64 "          Runoff coefficient      0.152  0.495  0.310  "
65 "          Maximum flow           0.001  0.008  0.009  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.009  0.000  0.000  0.000"
    
```

```

69 " 81      ADD COMMENT=====
70 "        2 Lines of comment"
71 "        IA increased to 20mm to account for roof and landscape area "
72 "        runoff reduction due to amended topsoil"
73 " 33      CATCHMENT 202"
74 "        1 Triangular SCS"
75 "        1 Equal length"
76 "        1 SCS method"
77 "        202 Controlled area to Highway 6"
78 "        70.000 % Impervious"
79 "        0.962 Total Area"
80 "        15.000 Flow length"
81 "        2.000 Overland Slope"
82 "        0.289 Pervious Area"
83 "        15.000 Pervious length"
84 "        2.000 Pervious slope"
85 "        0.673 Impervious Area"
86 "        15.000 Impervious length"
87 "        2.000 Impervious slope"
88 "        0.250 Pervious Manning 'n'"
89 "        75.000 Pervious SCS Curve No."
90 "        0.152 Pervious Runoff coefficient"
91 "        0.236 Pervious Ia/S coefficient"
92 "        19.981 Pervious Initial abstraction"
93 "        0.015 Impervious Manning 'n'"
94 "        98.000 Impervious SCS Curve No."
95 "        0.867 Impervious Runoff coefficient"
96 "        0.100 Impervious Ia/S coefficient"
97 "        0.518 Impervious Initial abstraction"
98 "        0.270 0.000 0.000 0.000 c.m/sec"
99 "        Catchment 202 Pervious Impervious Total Area "
100 "        Surface Area 0.289 0.673 0.962 hectare"
101 "        Time of concentration 19.542 1.162 2.448 minutes"
102 "        Time to Centroid 134.145 90.250 93.321 minutes"
103 "        Rainfall depth 49.226 49.226 49.226 mm"
104 "        Rainfall volume 142.07 331.49 473.55 c.m"
105 "        Rainfall losses 41.729 6.525 17.086 mm"
106 "        Runoff depth 7.497 42.701 32.140 mm"
107 "        Runoff volume 21.64 287.55 309.18 c.m"
108 "        Runoff coefficient 0.152 0.867 0.653 "
109 "        Maximum flow 0.005 0.270 0.270 c.m/sec"
110 " 40      HYDROGRAPH Add Runoff "
111 "        4 Add Runoff "
112 "        0.270 0.270 0.000 0.000"
113 " 54      POND DESIGN"
114 "        0.270 Current peak flow c.m/sec"
115 "        0.207 Target outflow c.m/sec"
116 "        309.2 Hydrograph volume c.m"
117 "        9. Number of stages"
118 "        421.990 Minimum water level metre"
119 "        424.030 Maximum water level metre"
120 "        421.990 Starting water level metre"
121 "        0 Keep Design Data: 1 = True; 0 = False"
122 "        Level Discharge Volume"
123 "        421.990 0.000 0.000"
124 "        422.200 0.00642 1.01E-05"
125 "        422.600 0.01201 85.000"
126 "        423.000 0.01572 170.000"
127 "        423.500 0.01939 211.987"
128 "        423.830 0.02147 221.426"
129 "        423.930 0.02206 239.726"
130 "        423.980 0.02235 270.251"
131 "        424.030 0.06480 325.201"
132 "        1. WEIRS"
133 "        Crest Weir Crest Left Right"
134 "        elevation coefficie breadth sideslope sideslope"
135 "        423.980 0.900 0.600 50.000 50.000"
136 "        1. ORIFICES"
    
```

137	"	Orifice	Orifice	Orifice	Number of	
138	"	invert	coefficie	diameter	orifices"	
139	"	421.990	0.820	0.0750	1.000"	
140	"	Peak outflow		0.017	c.m/sec"	
141	"	Maximum level		423.185	metre"	
142	"	Maximum storage		185.514	c.m"	
143	"	Centroidal lag		3.733	hours"	
144	"	0.270	0.270	0.017	0.000	c.m/sec"
145	"	40	HYDROGRAPH	Combine	1"	
146	"	6	Combine	"		
147	"	1	Node #"			
148	"		Total to Highway #6"			
149	"		Maximum flow	0.017	c.m/sec"	
150	"		Hydrograph volume	309.496	c.m"	
151	"		0.270	0.270	0.017	0.017"
152	"	40	HYDROGRAPH Start - New Tributary"			
153	"	2	Start - New Tributary"			
154	"		0.270	0.000	0.017	0.017"
155	"	81	ADD COMMENT=====			
156	"	2	Lines of comment"			
157	"		IA increased to 20mm to account for roof and landscape area "			
158	"		runoff reduction due to amended topsoil"			
159	"	33	CATCHMENT 203"			
160	"	1	Triangular SCS"			
161	"	1	Equal length"			
162	"	1	SCS method"			
163	"	203	Uncontrolled to Highway 6"			
164	"	23.000	% Impervious"			
165	"	0.304	Total Area"			
166	"	120.000	Flow length"			
167	"	2.000	Overland Slope"			
168	"	0.234	Pervious Area"			
169	"	120.000	Pervious length"			
170	"	2.000	Pervious slope"			
171	"	0.070	Impervious Area"			
172	"	120.000	Impervious length"			
173	"	2.000	Impervious slope"			
174	"	0.250	Pervious Manning 'n'"			
175	"	75.000	Pervious SCS Curve No."			
176	"	0.153	Pervious Runoff coefficient"			
177	"	0.236	Pervious Ia/S coefficient"			
178	"	19.981	Pervious Initial abstraction"			
179	"	0.015	Impervious Manning 'n'"			
180	"	98.000	Impervious SCS Curve No."			
181	"	0.501	Impervious Runoff coefficient"			
182	"	3.858	Impervious Ia/S coefficient"			
183	"	19.999	Impervious Initial abstraction"			
184	"		0.008	0.000	0.017	0.017 c.m/sec"
185	"		Catchment 203	Pervious	Impervious	Total Area "
186	"		Surface Area	0.234	0.070	0.304 hectare"
187	"		Time of concentration	68.049	5.923	37.281 minutes"
188	"		Time to Centroid	184.489	112.215	148.695 minutes"
189	"		Rainfall depth	49.226	49.226	49.226 mm"
190	"		Rainfall volume	115.23	34.42	149.65 c.m"
191	"		Rainfall losses	41.719	24.566	37.773 mm"
192	"		Runoff depth	7.507	24.660	11.453 mm"
193	"		Runoff volume	17.57	17.24	34.82 c.m"
194	"		Runoff coefficient	0.153	0.501	0.233 "
195	"		Maximum flow	0.002	0.008	0.008 c.m/sec"
196	"	40	HYDROGRAPH Add Runoff "			
197	"	4	Add Runoff "			
198	"		0.008	0.008	0.017	0.017"
199	"	40	HYDROGRAPH Copy to Outflow"			
200	"	8	Copy to Outflow"			
201	"		0.008	0.008	0.008	0.017"
202	"	40	HYDROGRAPH	Combine	1"	
203	"	6	Combine	"		
204	"	1	Node #"			

205 "	Total to Highway #6"				
206 "	Maximum flow	0.023	c.m/sec"		
207 "	Hydrograph volume	344.312	c.m"		
208 "	0.008 0.008	0.008	0.023"		
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area	1.266	hectare"		
212 "	Total Impervious area	0.743	hectare"		
213 "	Total % impervious	58.714"			
214 " 19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     25yr post r4.out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:               10/27/2023 at 3:58:24 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          702.000 Coefficient A"
17 "          0.350  Constant B"
18 "          0.690  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          220.574  mm/hr"
23 "          Total depth                 58.353  mm"
24 "          6  025hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000  % Impervious"
35 "          0.136  Total Area"
36 "          15.000  Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000  Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000  Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000  Pervious SCS Curve No."
46 "          0.205  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981  Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000  Impervious SCS Curve No."
51 "          0.564  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999  Impervious Initial abstraction"
54 "          0.016  0.000  0.000  0.000 c.m/sec"
55 "          Catchment 201  Pervious  Impervious Total Area "
56 "          Surface Area          0.073  0.063  0.136  hectare"
57 "          Time of concentration  13.765  1.331  5.044  minutes"
58 "          Time to Centroid       126.673  102.749  109.891  minutes"
59 "          Rainfall depth         58.353  58.353  58.353  mm"
60 "          Rainfall volume        42.85  36.51  79.36  c.m"
61 "          Rainfall losses        46.415  25.428  36.761  mm"
62 "          Runoff depth           11.938  32.924  21.592  mm"
63 "          Runoff volume           8.77  20.60  29.36  c.m"
64 "          Runoff coefficient      0.205  0.564  0.370  "
65 "          Maximum flow           0.002  0.015  0.016  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.016  0.000  0.000  0.000"
    
```

```

69 " 81      ADD COMMENT=====
70 "          2 Lines of comment"
71 "          IA increased to 20mm to account for roof and landscape area "
72 "          runoff reduction due to amended topsoil"
73 " 33      CATCHMENT 202"
74 "          1 Triangular SCS"
75 "          1 Equal length"
76 "          1 SCS method"
77 "          202 Controlled area to Highway 6"
78 "          70.000 % Impervious"
79 "          0.962 Total Area"
80 "          15.000 Flow length"
81 "          2.000 Overland Slope"
82 "          0.289 Pervious Area"
83 "          15.000 Pervious length"
84 "          2.000 Pervious slope"
85 "          0.673 Impervious Area"
86 "          15.000 Impervious length"
87 "          2.000 Impervious slope"
88 "          0.250 Pervious Manning 'n'"
89 "          75.000 Pervious SCS Curve No."
90 "          0.205 Pervious Runoff coefficient"
91 "          0.236 Pervious Ia/S coefficient"
92 "          19.981 Pervious Initial abstraction"
93 "          0.015 Impervious Manning 'n'"
94 "          98.000 Impervious SCS Curve No."
95 "          0.879 Impervious Runoff coefficient"
96 "          0.100 Impervious Ia/S coefficient"
97 "          0.518 Impervious Initial abstraction"
98 "          0.328 0.000 0.000 0.000 c.m/sec"
99 "          Catchment 202 Pervious Impervious Total Area "
100 "          Surface Area 0.289 0.673 0.962 hectare"
101 "          Time of concentration 13.765 1.081 2.232 minutes"
102 "          Time to Centroid 126.673 89.548 92.917 minutes"
103 "          Rainfall depth 58.353 58.353 58.353 mm"
104 "          Rainfall volume 168.41 392.95 561.35 c.m"
105 "          Rainfall losses 46.415 7.077 18.879 mm"
106 "          Runoff depth 11.938 51.276 39.474 mm"
107 "          Runoff volume 34.45 345.29 379.74 c.m"
108 "          Runoff coefficient 0.205 0.879 0.676 "
109 "          Maximum flow 0.010 0.326 0.328 c.m/sec"
110 " 40      HYDROGRAPH Add Runoff "
111 "          4 Add Runoff "
112 "          0.328 0.328 0.000 0.000"
113 " 54      POND DESIGN"
114 "          0.328 Current peak flow c.m/sec"
115 "          0.207 Target outflow c.m/sec"
116 "          379.7 Hydrograph volume c.m"
117 "          9. Number of stages"
118 "          421.990 Minimum water level metre"
119 "          424.030 Maximum water level metre"
120 "          421.990 Starting water level metre"
121 "          0 Keep Design Data: 1 = True; 0 = False"
122 "          Level Discharge Volume"
123 "          421.990 0.000 0.000"
124 "          422.200 0.00642 1.01E-05"
125 "          422.600 0.01201 85.000"
126 "          423.000 0.01572 170.000"
127 "          423.500 0.01939 211.987"
128 "          423.830 0.02147 221.426"
129 "          423.930 0.02206 239.726"
130 "          423.980 0.02235 270.251"
131 "          424.030 0.06480 325.201"
132 "          1. WEIRS"
133 "          Crest Weir Crest Left Right"
134 "          elevation coefficie breadth sideslope sideslope"
135 "          423.980 0.900 0.600 50.000 50.000"
136 "          1. ORIFICES"
    
```

```

137 "          Orifice Orifice Orifice Number of"
138 "          invert coefficie diameter orifices"
139 "          421.990 0.820 0.0750 1.000"
140 "          Peak outflow 0.022 c.m/sec"
141 "          Maximum level 423.882 metre"
142 "          Maximum storage 230.850 c.m"
143 "          Centroidal lag 3.849 hours"
144 "          0.328 0.328 0.022 0.000 c.m/sec"
145 " 40 HYDROGRAPH Combine 1"
146 " 6 Combine "
147 " 1 Node #"
148 "          Total to Highway #6"
149 "          Maximum flow 0.022 c.m/sec"
150 "          Hydrograph volume 379.436 c.m"
151 "          0.328 0.328 0.022 0.022"
152 " 40 HYDROGRAPH Start - New Tributary"
153 " 2 Start - New Tributary"
154 "          0.328 0.000 0.022 0.022"
155 " 81 ADD COMMENT=====
156 " 2 Lines of comment"
157 "          IA increased to 20mm to account for roof and landscape area "
158 "          runoff reduction due to amended topsoil"
159 " 33 CATCHMENT 203"
160 " 1 Triangular SCS"
161 " 1 Equal length"
162 " 1 SCS method"
163 " 203 Uncontrolled to Highway 6"
164 " 23.000 % Impervious"
165 " 0.304 Total Area"
166 " 120.000 Flow length"
167 " 2.000 Overland Slope"
168 " 0.234 Pervious Area"
169 " 120.000 Pervious length"
170 " 2.000 Pervious slope"
171 " 0.070 Impervious Area"
172 " 120.000 Impervious length"
173 " 2.000 Impervious slope"
174 " 0.250 Pervious Manning 'n'"
175 " 75.000 Pervious SCS Curve No."
176 " 0.205 Pervious Runoff coefficient"
177 " 0.236 Pervious Ia/S coefficient"
178 " 19.981 Pervious Initial abstraction"
179 " 0.015 Impervious Manning 'n'"
180 " 98.000 Impervious SCS Curve No."
181 " 0.574 Impervious Runoff coefficient"
182 " 3.858 Impervious Ia/S coefficient"
183 " 19.999 Impervious Initial abstraction"
184 "          0.015 0.000 0.022 0.022 c.m/sec"
185 "          Catchment 203 Pervious Impervious Total Area "
186 "          Surface Area 0.234 0.070 0.304 hectare"
187 "          Time of concentration 47.934 4.636 28.216 minutes"
188 "          Time to Centroid 167.633 107.838 140.402 minutes"
189 "          Rainfall depth 58.353 58.353 58.353 mm"
190 "          Rainfall volume 136.59 40.80 177.39 c.m"
191 "          Rainfall losses 46.389 24.859 41.437 mm"
192 "          Runoff depth 11.964 33.494 16.916 mm"
193 "          Runoff volume 28.01 23.42 51.43 c.m"
194 "          Runoff coefficient 0.205 0.574 0.290 "
195 "          Maximum flow 0.004 0.015 0.015 c.m/sec"
196 " 40 HYDROGRAPH Add Runoff "
197 " 4 Add Runoff "
198 "          0.015 0.015 0.022 0.022"
199 " 40 HYDROGRAPH Copy to Outflow"
200 " 8 Copy to Outflow"
201 "          0.015 0.015 0.015 0.022"
202 " 40 HYDROGRAPH Combine 1"
203 " 6 Combine "
204 " 1 Node #"
    
```

205 "	Total to Highway #6"				
206 "	Maximum flow	0.031	c.m/sec"		
207 "	Hydrograph volume	430.861	c.m"		
208 "	0.015 0.015	0.015	0.031"		
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area	1.266	hectare"		
212 "	Total Impervious area	0.743	hectare"		
213 "	Total % impervious	58.714"			
214 " 19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                     50yr post r4.out"
7 "          Licensee name:                       A"
8 "          Company                              "
9 "          Date & Time last used:               10/27/2023 at 3:57:05 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          780.000 Coefficient A"
17 "          0.360  Constant B"
18 "          0.690  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          244.972  mm/hr"
23 "          Total depth                65.003  mm"
24 "          6  050hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000  % Impervious"
35 "          0.136  Total Area"
36 "          15.000  Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000  Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000  Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000  Pervious SCS Curve No."
46 "          0.240  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981  Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000  Impervious SCS Curve No."
51 "          0.601  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999  Impervious Initial abstraction"
54 "          0.022  0.000  0.000  0.000 c.m/sec"
55 "          Catchment 201          Pervious  Impervious Total Area "
56 "          Surface Area          0.073  0.063  0.136  hectare"
57 "          Time of concentration  11.548  1.182  4.491  minutes"
58 "          Time to Centroid      122.851  101.068  108.021  minutes"
59 "          Rainfall depth        65.003  65.003  65.003  mm"
60 "          Rainfall volume       47.74  40.67  88.40  c.m"
61 "          Rainfall losses       49.392  25.916  38.593  mm"
62 "          Runoff depth          15.610  39.086  26.409  mm"
63 "          Runoff volume         11.46  24.45  35.92  c.m"
64 "          Runoff coefficient     0.240  0.601  0.406  "
65 "          Maximum flow          0.004  0.021  0.022  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.022  0.000  0.000  0.000"
    
```

```

69 " 81          ADD COMMENT=====
70 "           2 Lines of comment"
71 "           IA increased to 20mm to account for roof and landscape area "
72 "           runoff reduction due to amended topsoil"
73 " 33          CATCHMENT 202"
74 "           1 Triangular SCS"
75 "           1 Equal length"
76 "           1 SCS method"
77 "           202 Controlled area to Highway 6"
78 "           70.000 % Impervious"
79 "           0.962 Total Area"
80 "           15.000 Flow length"
81 "           2.000 Overland Slope"
82 "           0.289 Pervious Area"
83 "           15.000 Pervious length"
84 "           2.000 Pervious slope"
85 "           0.673 Impervious Area"
86 "           15.000 Impervious length"
87 "           2.000 Impervious slope"
88 "           0.250 Pervious Manning 'n'"
89 "           75.000 Pervious SCS Curve No."
90 "           0.240 Pervious Runoff coefficient"
91 "           0.236 Pervious Ia/S coefficient"
92 "           19.981 Pervious Initial abstraction"
93 "           0.015 Impervious Manning 'n'"
94 "           98.000 Impervious SCS Curve No."
95 "           0.885 Impervious Runoff coefficient"
96 "           0.100 Impervious Ia/S coefficient"
97 "           0.518 Impervious Initial abstraction"
98 "           0.370 0.000 0.000 0.000 c.m/sec"
99 "           Catchment 202 Pervious Impervious Total Area "
100 "           Surface Area 0.289 0.673 0.962 hectare"
101 "           Time of concentration 11.548 1.034 2.130 minutes"
102 "           Time to Centroid 122.851 89.143 92.655 minutes"
103 "           Rainfall depth 65.003 65.003 65.003 mm"
104 "           Rainfall volume 187.60 437.73 625.32 c.m"
105 "           Rainfall losses 49.392 7.474 20.050 mm"
106 "           Runoff depth 15.610 57.528 44.953 mm"
107 "           Runoff volume 45.05 387.39 432.45 c.m"
108 "           Runoff coefficient 0.240 0.885 0.692 "
109 "           Maximum flow 0.014 0.366 0.370 c.m/sec"
110 " 40          HYDROGRAPH Add Runoff "
111 "           4 Add Runoff "
112 "           0.370 0.370 0.000 0.000"
113 " 54          POND DESIGN"
114 "           0.370 Current peak flow c.m/sec"
115 "           0.207 Target outflow c.m/sec"
116 "           432.4 Hydrograph volume c.m"
117 "           9. Number of stages"
118 "           421.990 Minimum water level metre"
119 "           424.030 Maximum water level metre"
120 "           421.990 Starting water level metre"
121 "           0 Keep Design Data: 1 = True; 0 = False"
122 "           Level Discharge Volume"
123 "           421.990 0.000 0.000"
124 "           422.200 0.00642 1.01E-05"
125 "           422.600 0.01201 85.000"
126 "           423.000 0.01572 170.000"
127 "           423.500 0.01939 211.987"
128 "           423.830 0.02147 221.426"
129 "           423.930 0.02206 239.726"
130 "           423.980 0.02235 270.251"
131 "           424.030 0.06480 325.201"
132 "           1. WEIRS"
133 "           Crest Weir Crest Left Right"
134 "           elevation coefficie breadth sideslope sideslope"
135 "           423.980 0.900 0.600 50.000 50.000"
136 "           1. ORIFICES"
    
```

```

137 "           Orifice Orifice Orifice Number of"
138 "           invert coefficie diameter orifices"
139 "           421.990 0.820 0.0750 1.000"
140 "           Peak outflow 0.022 c.m/sec"
141 "           Maximum level 423.980 metre"
142 "           Maximum storage 270.403 c.m"
143 "           Centroidal lag 4.044 hours"
144 "           0.370 0.370 0.022 0.000 c.m/sec"
145 " 40 HYDROGRAPH Combine 1"
146 " 6 Combine "
147 " 1 Node #"
148 "           Total to Highway #6"
149 "           Maximum flow 0.022 c.m/sec"
150 "           Hydrograph volume 432.895 c.m"
151 "           0.370 0.370 0.022 0.022"
152 " 40 HYDROGRAPH Start - New Tributary"
153 " 2 Start - New Tributary"
154 "           0.370 0.000 0.022 0.022"
155 " 81 ADD COMMENT=====
156 " 2 Lines of comment"
157 "           IA increased to 20mm to account for roof and landscape area "
158 "           runoff reduction due to amended topsoil"
159 " 33 CATCHMENT 203"
160 " 1 Triangular SCS"
161 " 1 Equal length"
162 " 1 SCS method"
163 " 203 Uncontrolled to Highway 6"
164 " 23.000 % Impervious"
165 " 0.304 Total Area"
166 " 120.000 Flow length"
167 " 2.000 Overland Slope"
168 " 0.234 Pervious Area"
169 " 120.000 Pervious length"
170 " 2.000 Pervious slope"
171 " 0.070 Impervious Area"
172 " 120.000 Impervious length"
173 " 2.000 Impervious slope"
174 " 0.250 Pervious Manning 'n'"
175 " 75.000 Pervious SCS Curve No."
176 " 0.240 Pervious Runoff coefficient"
177 " 0.236 Pervious Ia/S coefficient"
178 " 19.981 Pervious Initial abstraction"
179 " 0.015 Impervious Manning 'n'"
180 " 98.000 Impervious SCS Curve No."
181 " 0.612 Impervious Runoff coefficient"
182 " 3.858 Impervious Ia/S coefficient"
183 " 19.999 Impervious Initial abstraction"
184 "           0.021 0.000 0.022 0.022 c.m/sec"
185 "           Catchment 203 Pervious Impervious Total Area "
186 "           Surface Area 0.234 0.070 0.304 hectare"
187 "           Time of concentration 40.214 4.116 24.626 minutes"
188 "           Time to Centroid 159.258 105.832 136.187 minutes"
189 "           Rainfall depth 65.003 65.003 65.003 mm"
190 "           Rainfall volume 152.16 45.45 197.61 c.m"
191 "           Rainfall losses 49.377 25.243 43.826 mm"
192 "           Runoff depth 15.626 39.760 21.177 mm"
193 "           Runoff volume 36.58 27.80 64.38 c.m"
194 "           Runoff coefficient 0.240 0.612 0.326 "
195 "           Maximum flow 0.005 0.020 0.021 c.m/sec"
196 " 40 HYDROGRAPH Add Runoff "
197 " 4 Add Runoff "
198 "           0.021 0.021 0.022 0.022"
199 " 40 HYDROGRAPH Copy to Outflow"
200 " 8 Copy to Outflow"
201 "           0.021 0.021 0.021 0.022"
202 " 40 HYDROGRAPH Combine 1"
203 " 6 Combine "
204 " 1 Node #"
    
```

205 "	Total to Highway #6"				
206 "	Maximum flow	0.038	c.m/sec"		
207 "	Hydrograph volume	497.272	c.m"		
208 "	0.021 0.021	0.021	0.038"		
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area	1.266	hectare"		
212 "	Total Impervious area	0.743	hectare"		
213 "	Total % impervious	58.714"			
214 " 19	EXIT"				

```

1 "          MIDUSS Output ----->"
2 "          MIDUSS version                      Version 2.25  rev. 473"
3 "          MIDUSS created                      Sunday, February 7, 2010"
4 "          10  Units used:                      ie METRIC"
5 "          Job folder:                          Q:\48650\100\SWM"
6 "          Output filename:                    100yr post r4.out"
7 "          Licensee name:                      A"
8 "          Company                             "
9 "          Date & Time last used:              10/27/2023 at 3:48:01 PM"
10 " 31      TIME PARAMETERS"
11 "          5.000  Time Step"
12 "          180.000 Max. Storm length"
13 "          1500.000 Max. Hydrograph"
14 " 32      STORM Chicago storm"
15 "          1  Chicago storm"
16 "          851.000 Coefficient A"
17 "          0.290  Constant B"
18 "          0.687  Exponent C"
19 "          0.400  Fraction R"
20 "          180.000 Duration"
21 "          1.000  Time step multiplier"
22 "          Maximum intensity          270.786  mm/hr"
23 "          Total depth                71.828  mm"
24 "          6  100hyd  Hydrograph extension used in this file"
25 " 81      ADD COMMENT-----"
26 "          2  Lines of comment"
27 "          IA increased to 20mm to account for roof and landscape area "
28 "          runoff reduction due to amended topsoil"
29 " 33      CATCHMENT 201"
30 "          1  Triangular SCS"
31 "          1  Equal length"
32 "          1  SCS method"
33 "          201  Area to southwest property line, ultimately to Mun Drain #1"
34 "          46.000  % Impervious"
35 "          0.136  Total Area"
36 "          15.000  Flow length"
37 "          2.000  Overland Slope"
38 "          0.073  Pervious Area"
39 "          15.000  Pervious length"
40 "          2.000  Pervious slope"
41 "          0.063  Impervious Area"
42 "          15.000  Impervious length"
43 "          2.000  Impervious slope"
44 "          0.250  Pervious Manning 'n'"
45 "          75.000  Pervious SCS Curve No."
46 "          0.272  Pervious Runoff coefficient"
47 "          0.236  Pervious Ia/S coefficient"
48 "          19.981  Pervious Initial abstraction"
49 "          0.015  Impervious Manning 'n'"
50 "          98.000  Impervious SCS Curve No."
51 "          0.631  Impervious Runoff coefficient"
52 "          3.858  Impervious Ia/S coefficient"
53 "          19.999  Impervious Initial abstraction"
54 "          0.029  0.000  0.000  0.000 c.m/sec"
55 "          Catchment 201  Pervious  Impervious  Total Area  "
56 "          Surface Area  0.073  0.063  0.136  hectare"
57 "          Time of concentration  10.001  1.074  4.076  minutes"
58 "          Time to Centroid  120.070  99.883  106.671  minutes"
59 "          Rainfall depth  71.828  71.828  71.828  mm"
60 "          Rainfall volume  52.75  44.94  97.69  c.m"
61 "          Rainfall losses  52.256  26.477  40.398  mm"
62 "          Runoff depth  19.572  45.352  31.431  mm"
63 "          Runoff volume  14.37  28.37  42.75  c.m"
64 "          Runoff coefficient  0.272  0.631  0.438  "
65 "          Maximum flow  0.005  0.028  0.029  c.m/sec"
66 " 40      HYDROGRAPH Start - New Tributary"
67 "          2  Start - New Tributary"
68 "          0.029  0.000  0.000  0.000"
    
```

```

69 " 81          ADD COMMENT=====
70 "          2 Lines of comment"
71 "          IA increased to 20mm to account for roof and landscape area "
72 "          runoff reduction due to amended topsoil"
73 " 33          CATCHMENT 202"
74 "          1 Triangular SCS"
75 "          1 Equal length"
76 "          1 SCS method"
77 "          202 Controlled area to Highway 6"
78 "          70.000 % Impervious"
79 "          0.962 Total Area"
80 "          15.000 Flow length"
81 "          2.000 Overland Slope"
82 "          0.289 Pervious Area"
83 "          15.000 Pervious length"
84 "          2.000 Pervious slope"
85 "          0.673 Impervious Area"
86 "          15.000 Impervious length"
87 "          2.000 Impervious slope"
88 "          0.250 Pervious Manning 'n'"
89 "          75.000 Pervious SCS Curve No."
90 "          0.272 Pervious Runoff coefficient"
91 "          0.236 Pervious Ia/S coefficient"
92 "          19.981 Pervious Initial abstraction"
93 "          0.015 Impervious Manning 'n'"
94 "          98.000 Impervious SCS Curve No."
95 "          0.890 Impervious Runoff coefficient"
96 "          0.100 Impervious Ia/S coefficient"
97 "          0.518 Impervious Initial abstraction"
98 "          0.414 0.000 0.000 0.000 c.m/sec"
99 "          Catchment 202 Pervious Impervious Total Area "
100 "          Surface Area 0.289 0.673 0.962 hectare"
101 "          Time of concentration 10.001 0.992 2.037 minutes"
102 "          Time to Centroid 120.070 88.820 92.444 minutes"
103 "          Rainfall depth 71.828 71.828 71.828 mm"
104 "          Rainfall volume 207.30 483.69 690.99 c.m"
105 "          Rainfall losses 52.256 7.885 21.197 mm"
106 "          Runoff depth 19.572 63.943 50.632 mm"
107 "          Runoff volume 56.49 430.59 487.08 c.m"
108 "          Runoff coefficient 0.272 0.890 0.705 "
109 "          Maximum flow 0.020 0.409 0.414 c.m/sec"
110 " 40          HYDROGRAPH Add Runoff "
111 "          4 Add Runoff "
112 "          0.414 0.414 0.000 0.000"
113 " 54          POND DESIGN"
114 "          0.414 Current peak flow c.m/sec"
115 "          0.207 Target outflow c.m/sec"
116 "          487.1 Hydrograph volume c.m"
117 "          9. Number of stages"
118 "          421.990 Minimum water level metre"
119 "          424.030 Maximum water level metre"
120 "          421.990 Starting water level metre"
121 "          0 Keep Design Data: 1 = True; 0 = False"
122 "          Level Discharge Volume"
123 "          421.990 0.000 0.000"
124 "          422.200 0.00642 1.01E-05"
125 "          422.600 0.01201 85.000"
126 "          423.000 0.01572 170.000"
127 "          423.500 0.01939 211.987"
128 "          423.830 0.02147 221.426"
129 "          423.930 0.02206 239.726"
130 "          423.980 0.02235 270.251"
131 "          424.030 0.06480 325.201"
132 "          1. WEIRS"
133 "          Crest Weir Crest Left Right"
134 "          elevation coefficie breadth sideslope sideslope"
135 "          423.980 0.900 0.600 50.000 50.000"
136 "          1. ORIFICES"
    
```

137	"	Orifice	Orifice	Orifice	Number of	
138	"	invert	coefficie	diameter	orifices"	
139	"	421.990	0.820	0.0750	1.000"	
140	"	Peak outflow		0.037	c.m/sec"	
141	"	Maximum level		423.998	metre"	
142	"	Maximum storage		289.708	c.m"	
143	"	Centroidal lag		3.888	hours"	
144	"	0.414	0.414	0.037	0.000	c.m/sec"
145	"	40	HYDROGRAPH	Combine	1"	
146	"	6	Combine	"		
147	"	1	Node #"			
148	"		Total to Highway #6"			
149	"		Maximum flow	0.037	c.m/sec"	
150	"		Hydrograph volume	486.912	c.m"	
151	"		0.414	0.414	0.037	0.037"
152	"	40	HYDROGRAPH Start - New Tributary"			
153	"	2	Start - New Tributary"			
154	"		0.414	0.000	0.037	0.037"
155	"	81	ADD COMMENT=====			
156	"	2	Lines of comment"			
157	"		IA increased to 20mm to account for roof and landscape area "			
158	"		runoff reduction due to amended topsoil"			
159	"	33	CATCHMENT 203"			
160	"	1	Triangular SCS"			
161	"	1	Equal length"			
162	"	1	SCS method"			
163	"	203	Uncontrolled to Highway 6"			
164	"	23.000	% Impervious"			
165	"	0.304	Total Area"			
166	"	120.000	Flow length"			
167	"	2.000	Overland Slope"			
168	"	0.234	Pervious Area"			
169	"	120.000	Pervious length"			
170	"	2.000	Pervious slope"			
171	"	0.070	Impervious Area"			
172	"	120.000	Impervious length"			
173	"	2.000	Impervious slope"			
174	"	0.250	Pervious Manning 'n'"			
175	"	75.000	Pervious SCS Curve No."			
176	"	0.274	Pervious Runoff coefficient"			
177	"	0.236	Pervious Ia/S coefficient"			
178	"	19.981	Pervious Initial abstraction"			
179	"	0.015	Impervious Manning 'n'"			
180	"	98.000	Impervious SCS Curve No."			
181	"	0.639	Impervious Runoff coefficient"			
182	"	3.858	Impervious Ia/S coefficient"			
183	"	19.999	Impervious Initial abstraction"			
184	"		0.026	0.000	0.037	0.037 c.m/sec"
185	"		Catchment 203	Pervious	Impervious	Total Area "
186	"		Surface Area	0.234	0.070	0.304 hectare"
187	"		Time of concentration	34.827	3.740	22.058 minutes"
188	"		Time to Centroid	152.796	104.435	132.933 minutes"
189	"		Rainfall depth	71.828	71.828	71.828 mm"
190	"		Rainfall volume	168.14	50.22	218.36 c.m"
191	"		Rainfall losses	52.152	25.915	46.118 mm"
192	"		Runoff depth	19.676	45.913	25.711 mm"
193	"		Runoff volume	46.06	32.10	78.16 c.m"
194	"		Runoff coefficient	0.274	0.639	0.358 "
195	"		Maximum flow	0.008	0.024	0.026 c.m/sec"
196	"	40	HYDROGRAPH Add Runoff "			
197	"	4	Add Runoff "			
198	"		0.026	0.026	0.037	0.037"
199	"	40	HYDROGRAPH Copy to Outflow"			
200	"	8	Copy to Outflow"			
201	"		0.026	0.026	0.026	0.037"
202	"	40	HYDROGRAPH	Combine	1"	
203	"	6	Combine	"		
204	"	1	Node #"			

205 "	Total to Highway #6"				
206 "	Maximum flow		0.048	c.m/sec"	
207 "	Hydrograph volume		565.072	c.m"	
208 "	0.026 0.026		0.026	0.048"	
209 " 38	START/RE-START TOTALS 203"				
210 "	3 Runoff Totals on EXIT"				
211 "	Total Catchment area		1.266	hectare"	
212 "	Total Impervious area		0.743	hectare"	
213 "	Total % impervious		58.714"		
214 " 19	EXIT"				

Appendix C

Stormceptor Sizing

Stormceptor® EF Sizing Report

**STORMCEPTOR®
ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION**

05/10/2022

Province:	Ontario
City:	Fergus
Nearest Rainfall Station:	WATERLOO WELLINGTON AP
Climate Station Id:	6149387
Years of Rainfall Data:	34

Project Name:	961 St. David Street North
Project Number:	48650-100
Designer Name:	Nathan Katerberg
Designer Company:	MTE Consultants Inc
Designer Email:	nkaterberg@mte85.com
Designer Phone:	519-743-6500
EOR Name:	
EOR Company:	
EOR Email:	
EOR Phone:	

Site Name:	961 St. David Street North
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Drainage Area (ha):	0.77
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% Imperviousness:	75.00
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Runoff Coefficient 'c': 0.75

Particle Size Distribution:	Fine
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Target TSS Removal (%):	80.0
-------------------------	------

Required Water Quality Runoff Volume Capture (%):	90.00
---	-------

Estimated Water Quality Flow Rate (L/s):	21.88
--	-------

Oil / Fuel Spill Risk Site?	Yes
-----------------------------	-----

Upstream Flow Control?	Yes
------------------------	-----

Upstream Orifice Control Flow Rate to Stormceptor (L/s):	22.00
--	-------

Peak Conveyance (maximum) Flow Rate (L/s):	
--	--

Site Sediment Transport Rate (kg/ha/yr):	
--	--

Net Annual Sediment (TSS) Load Reduction Sizing Summary	
Stormceptor Model	TSS Removal Provided (%)
EFO4	80
EFO6	89
EFO8	95
EFO10	97
EFO12	99

Recommended Stormceptor EFO Model: EFO4
Estimated Net Annual Sediment (TSS) Load Reduction (%): 80
Water Quality Runoff Volume Capture (%): > 90



Stormceptor® EF Sizing Report

THIRD-PARTY TESTING AND VERIFICATION

► **Stormceptor® EF and Stormceptor® EFO** are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** and performance has been third-party verified in accordance with the **ISO 14034 Environmental Technology Verification (ETV)** protocol.

PERFORMANCE

► **Stormceptor® EF and EFO** remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

PARTICLE SIZE DISTRIBUTION (PSD)

► The **Canadian ETV PSD** shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators** for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (µm)	Percent Less Than	Particle Size Fraction (µm)	Percent
1000	100	500-1000	5
500	95	250-500	5
250	90	150-250	15
150	75	100-150	15
100	60	75-100	10
75	50	50-75	5
50	45	20-50	10
20	35	8-20	15
8	20	5-8	10
5	10	2-5	5
2	5	<2	5

Stormceptor®EF Sizing Report

Upstream Flow Controlled Results

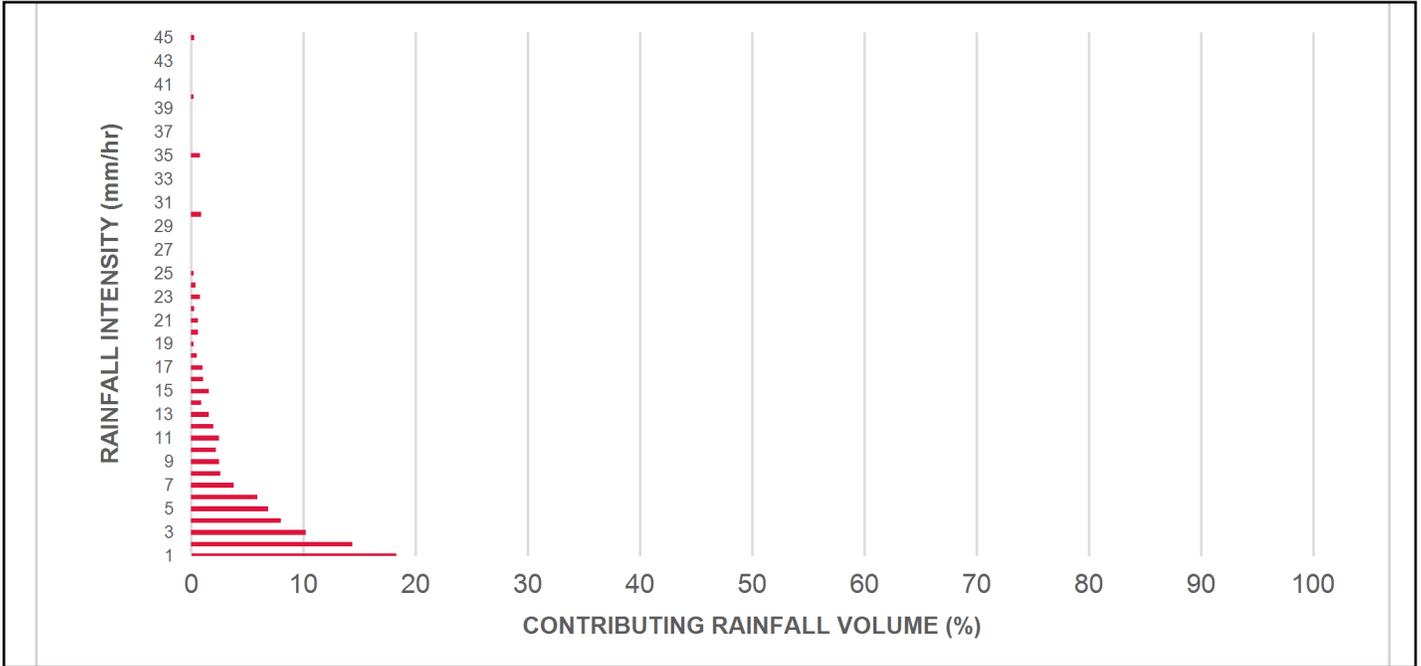
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m ²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.5	8.5	8.5	0.80	48.0	40.0	100	8.5	8.5
1	18.3	26.8	1.61	96.0	80.0	98	18.0	26.5
2	14.4	41.3	3.21	193.0	161.0	88	12.7	39.3
3	10.2	51.5	4.82	289.0	241.0	81	8.3	47.6
4	8.0	59.5	6.42	385.0	321.0	78	6.2	53.8
5	6.9	66.4	8.03	482.0	401.0	74	5.1	58.9
6	5.9	72.3	9.63	578.0	482.0	70	4.1	63.0
7	3.8	76.1	11.24	674.0	562.0	66	2.5	65.5
8	2.6	78.7	12.84	771.0	642.0	64	1.7	67.2
9	2.5	81.1	14.45	867.0	722.0	64	1.6	68.8
10	2.2	83.3	16.05	963.0	803.0	63	1.4	70.1
11	2.5	85.8	17.66	1060.0	883.0	62	1.6	71.7
12	2.0	87.8	19.27	1156.0	963.0	62	1.2	72.9
13	12.2	100.0	20.87	1252.0	1044.0	61	7.4	80.3
14	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
15	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
16	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
17	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
18	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
19	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
20	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
21	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
22	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
23	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
24	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
25	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
30	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
35	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
40	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
45	0.0	100.0	22.00	1320.0	1100.0	59	0.0	80.3
Estimated Net Annual Sediment (TSS) Load Reduction =								80 %

Climate Station ID: 6149387 Years of Rainfall Data: 34

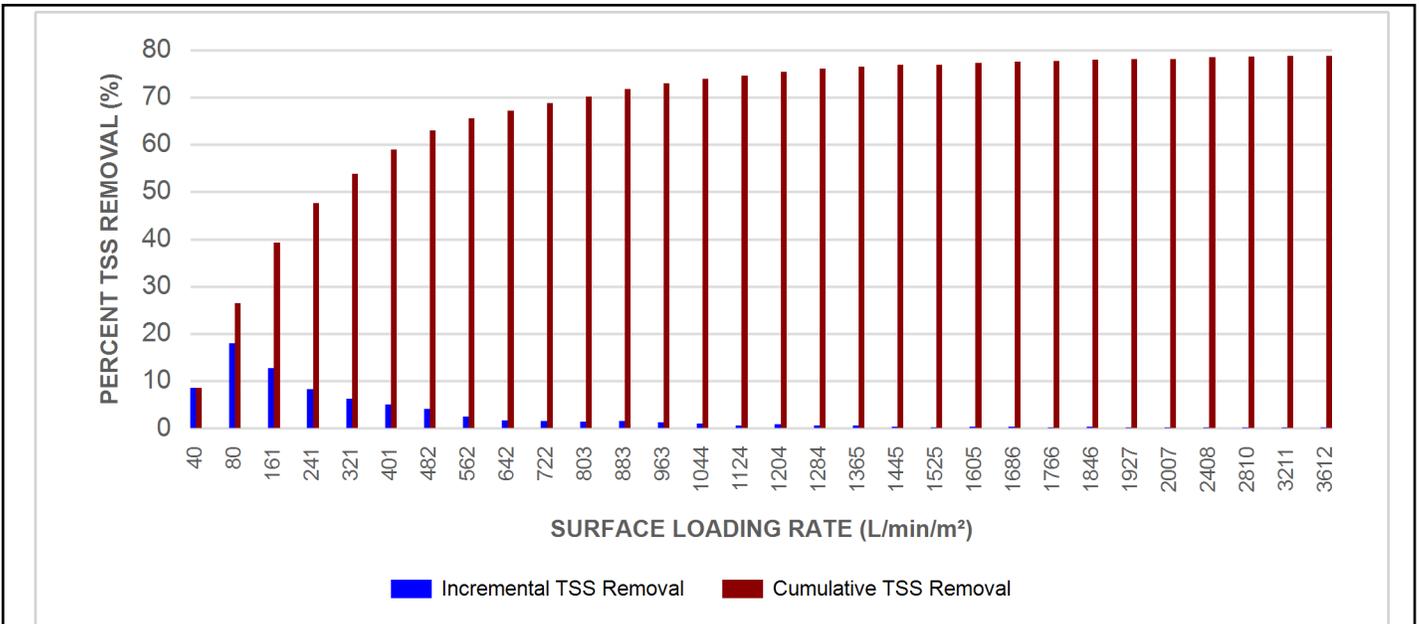


Stormceptor® EF Sizing Report

RAINFALL DATA FROM WATERLOO WELLINGTON AP RAINFALL STATION



INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL



Stormceptor® **EF** Sizing Report

Maximum Pipe Diameter / Peak Conveyance

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

SCOUR PREVENTION AND ONLINE CONFIGURATION

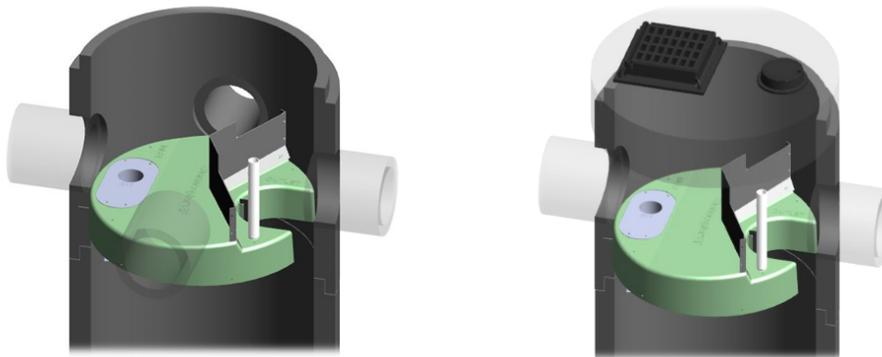
► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

DESIGN FLEXIBILITY

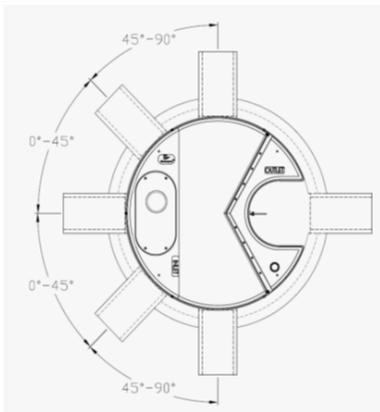
► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

OIL CAPTURE AND RETENTION

► While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, Stormceptor® EFO has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid re-entrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.



Stormceptor® EF Sizing Report



INLET-TO-OUTLET DROP

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

0° - 45° : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90° : The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

HEAD LOSS

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1.

For submerged conditions the applicable K value is 3.0.

Pollutant Capacity

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Volume		Recommended Sediment Maintenance Depth *		Maximum Sediment Volume *		Maximum Sediment Mass **	
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft ³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

*Increased sump depth may be added to increase sediment storage capacity

** Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit <http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef>

Stormceptor® **EF** Sizing Report

**STANDARD PERFORMANCE SPECIFICATION FOR
“OIL GRIT SEPARATOR” (OGS) STORMWATER QUALITY TREATMENT DEVICE**

PART 1 – GENERAL

1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program’s **Procedure for Laboratory Testing of Oil-Grit Separators**

1.3 SUBMITTALS

1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.

1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.

1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

PART 2 – PRODUCTS

2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The minimum sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1	4 ft (1219 mm) Diameter OGS Units:	1.19 m ³ sediment / 265 L oil
	6 ft (1829 mm) Diameter OGS Units:	3.48 m ³ sediment / 609 L oil
	8 ft (2438 mm) Diameter OGS Units:	8.78 m ³ sediment / 1,071 L oil
	10 ft (3048 mm) Diameter OGS Units:	17.78 m ³ sediment / 1,673 L oil
	12 ft (3657 mm) Diameter OGS Units:	31.23 m ³ sediment / 2,476 L oil

PART 3 – PERFORMANCE & DESIGN

3.1 GENERAL

The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall



Stormceptor® EF Sizing Report

remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.

3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.

3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².

3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m².

3.4 LIGHT LIQUID RE-ENTRAINMENT SIMULATION TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of completed third-party Light Liquid Re-entrainment Simulation Testing in accordance with the Canadian ETV **Program's Procedure for Laboratory Testing of Oil-Grit Separators**, with results reported within the Canadian ETV or ISO 14034 ETV verification. This re-entrainment testing is conducted with the device pre-loaded with low density polyethylene (LDPE) plastic beads as a surrogate for light liquids such as oil and fuel. Testing is conducted on the same OGS unit tested for sediment removal to

Stormceptor® EF Sizing Report

assess whether light liquids captured after a spill are effectively retained at high flow rates.

3.4.1 For an OGS device to be an acceptable stormwater treatment device on a site where vehicular traffic occurs and the potential for an oil or fuel spill exists, the OGS device must have reported verified performance results of greater than 99% cumulative retention of LDPE plastic beads for the five specified surface loading rates (ranging 200 L/min/m² to 2600 L/min/m²) in accordance with the Light Liquid Re-entrainment Simulation Testing within the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**. However, an OGS device shall not be allowed if the Light Liquid Re-entrainment Simulation Testing was performed with screening components within the OGS device that are effective at retaining the LDPE plastic beads, but would not be expected to retain light liquids such as oil and fuel.

Appendix D

Water Balance

961 ST. DAVID STREET
WATER BALANCE (SURFACE RUNOFF AND INFILTRATION) ANALYSIS
 Fergus, Ontario

Project No. 48650-100
 Date: October 28, 2023
 Design By: NGK
 File: Q:\48650\100\SWM\Water Balance\2023-09-28_Yearly Water

Weather Station Fergus Shand Dam, 1981-2010 Canada Climate Normals
 Total Precipitation 946 mm/year

Annual Water Balance Parameters & Hydrologic Cycle Components							
Condition	Topography	Coverage	Soil Type	ET (mm/yr)	Runoff (mm/yr)	Infiltration (mm/yr)	Notes
Pre-Development pervious areas	Flat Lands	Pasture/ Shrubs	A/B - Sand, Sandy Silt	588	71	287	
Impervious areas (Pre- and Post Development)				142	804	0	Evapotranspiration rate of 15% assumed for impervious areas
Post-Development pervious areas	Flat Lands	Urban Lawns	A/B - Sand, Sandy Silt	572	112	262	
Townhouse Lots with Amended Topsoil				288	363	295	Based on GAWSER modelling completed for typical townhouse lot coverage and grading, with runoff from roof and rear-yard areas draining to an amended topsoil reservoir in the rear yards. These rates are representative of the entire lot area.
Single Detached Lots with Amended Topsoil				341	85	520	Based on GAWSER modelling completed for typical single detached lot coverage and split drainage grading, with runoff from roof and rear-yard areas draining to an amended topsoil reservoir in the side and rear yards. These rates are representative of the entire lot area.

RUNOFF

Pre-Development Runoff										
Catchment ¹	Area	% Impervious	Pervious Area			Impervious Area			Total Runoff Volume	Comments
			Area	Runoff Rate ²	Runoff Volume	Area	Runoff Rate	Runoff Volume		
	ha		ha	mm/yr/m ²	m ³ /yr	ha	mm/yr/m ²	m ³ /yr	m ³ /yr	
301	0.804	0	0.804	71	571				571	To Wetland
302	0.598	9	0.544	71	386	0.054	804	433	819	To St. David Street North/Highway 6
Sum of Pre-Development Runoff									1,390	

Post-Development Runoff										
Catchment ¹	Area	% Impervious	Pervious Area			Impervious Area			Total Runoff Volume	Comments
			Area	Runoff Rate ²	Runoff Volume	Area	Runoff Rate ²	Runoff Volume		
	ha		ha	mm/yr/m ²	m ³ /yr	ha	mm/yr/m ²	m ³ /yr	m ³ /yr	
401	0.136	46	0.073	363	267	0.063	363	227	494	Townhouse Lots w/Amended Topsoil
Post-Development Runoff, to Wetland									494	
402-1	0.485	69	0.150	112	168	0.335	804	2,691	2,859	Common element, front roofs and yards of Catchment 401 townhouse lots
402-2	0.399	60	0.160	363	580	0.239	363	870	1,449	Townhouse Lots w/Amended Topsoil
403	0.382	43	0.218	85	185	0.164	85	140	325	Single Detached Lots w/Amended Topsoil
Post-Development Runoff, to St. David Street North/Highway 6									5,621	

INFILTRATION

Pre-Development Infiltration										
Catchment ¹	Area	% Impervious	Pervious Area			Impervious Area			Total Infiltration Volume	Comments
			Area	Infiltration Rate	Infiltration Volume	Area	Infiltration Rate	Infiltration Volume		
	ha		ha	mm/yr/m ²	m ³ /yr	ha	mm/yr/m ²	m ³ /yr	m ³ /yr	
301	0.804	0	0.804	287	2,307				2,307	To Wetland
302	0.598	9	0.544	287	1,562	0.054	0	0	1,562	To St. David Street North/Highway 6
Sum of Pre-Development Infiltration									3,869	

Post-Development Infiltration										
Catchment ¹	Area	% Impervious	Pervious Area			Impervious Area			Total Infiltration Volume	Comments
			Area	Infiltration Rate ²	Infiltration Volume	Area	Infiltration Rate ²	Infiltration Volume		
	ha		ha	mm/yr/m ²	m ³ /yr	ha	mm/yr/m ²	m ³ /yr	m ³ /yr	
401	0.136	46	0.073	295	217	0.063	295	185	401	Townhouse Lots w/Amended Topsoil
402-1	0.485	69	0.150	262	394				394	Common element, front roofs and yards of Catchment 401 townhouse lots
402-2	0.399	60	0.160	295	471	0.239	295	707	1,178	Townhouse Lots w/Amended Topsoil
403	0.382	43	0.218	520	1,133	0.164	520	855	1,988	Single Detached Lots w/Amended Topsoil
Sum of Post-Development Infiltration									3,961	

SUMMARY

		Pre-Development	Post-Development	Volume Change	Percentage Change
Runoff Volume (m ³ /yr)	To Wetland	571	494	-77 m3 increase	-14%
	To St. David Street/Highway 6	819	5,621	4,802 m3 increase	-
Infiltration Volume (m ³ /yr)		3,869	3,961	91 m3 increase	2%

NOTES

- Refer to Figures 2.0 and 4.0 for Pre- and Post-Development Water Balance Catchment Areas.
- Infiltration and runoff rates for Catchments 402-2 and 403 are based on GAWSER modelling of typical lot coverages and grading design for both townhouse lots and single detached split drainage lots, with runoff from the roof and rear yard areas draining to an amended topsoil reservoir. The GAWSER modelling routed runoff from the impervious roof areas through the amended topsoil reservoir, and determined infiltration and runoff rates representative of the entire lot. Therefore in the Infiltration and Runoff tables, the whole-lot rate is applied to both the Impervious and Pervious portions of Catchments 402-2 and 403